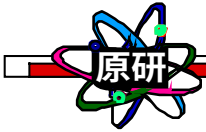


SiC Tokamak Reactor in JAERI



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JAERI

International Town Meeting on SiC/SiC Design and Material Issues for Fusion Systems
Jan.18-19, 2000, Oak Ridge National Laboratory, USA

CONTENTS

1. Material Requirements and Reactor Concept
2. Material Performance Comparison
3. Examples of SiC/SiC Blanket and Divertor
4. Limitation of SiC/SiC Application
5. Material Use Optimization
6. Summary

S. Nishio

Japan Atomic Energy Research Institute
Naka Fusion Establishment

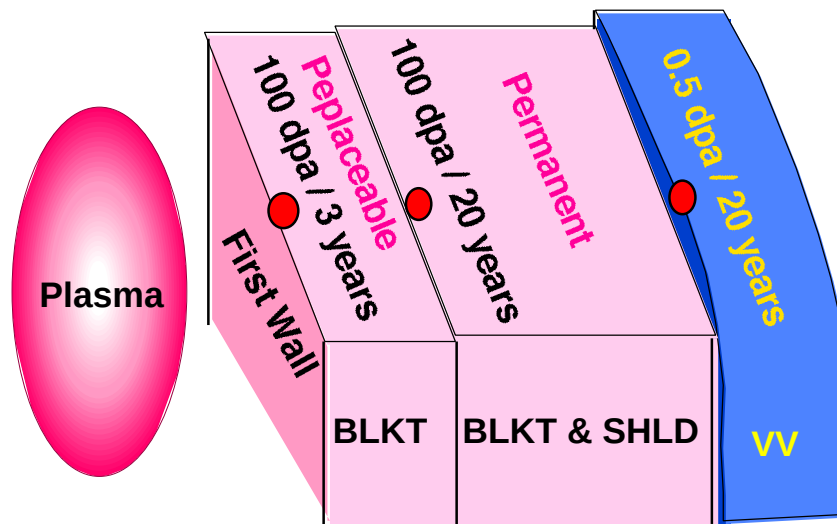
Fusion Material Development



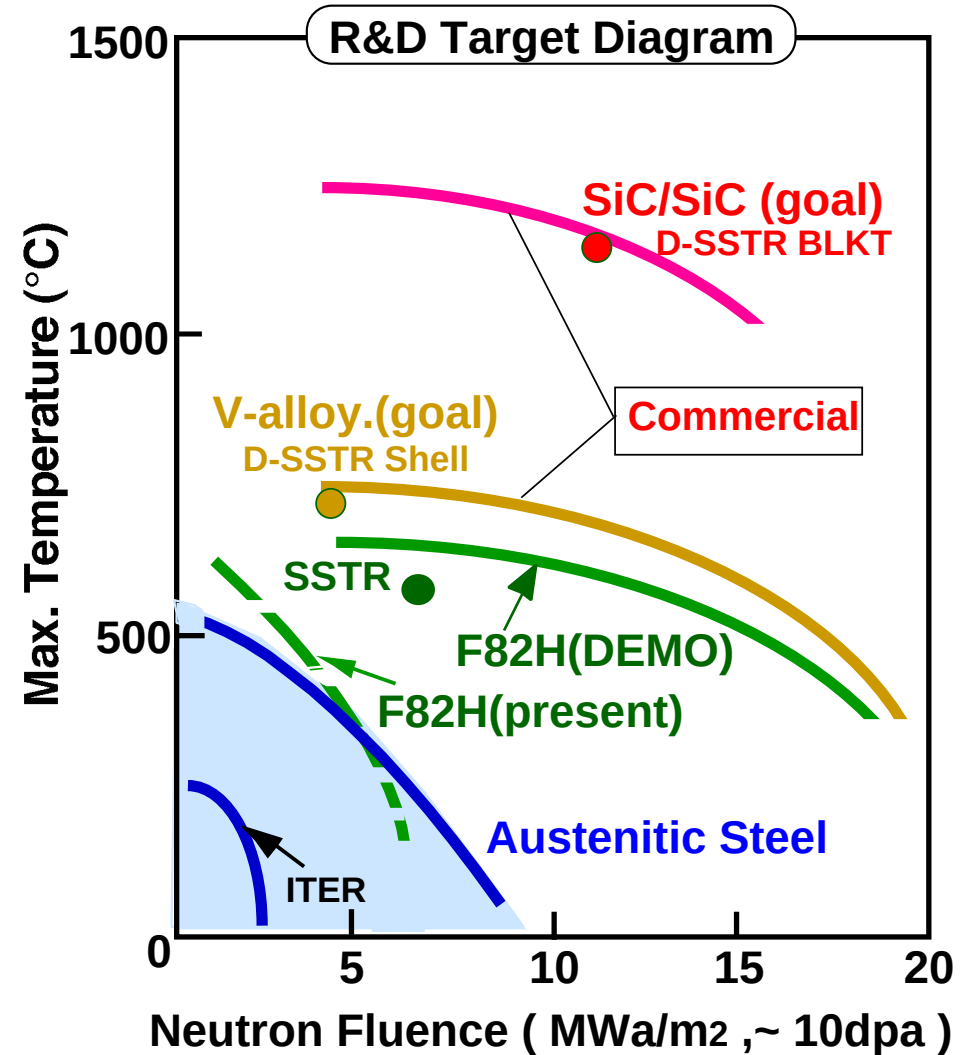
- 2 -

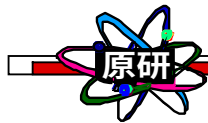
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- LA Ferritic Steel (1st Candi. for DEMO)
- V-alloy (Candi. for Comm.)
- SiC/SiC Comp. (Candi. for Comm.)



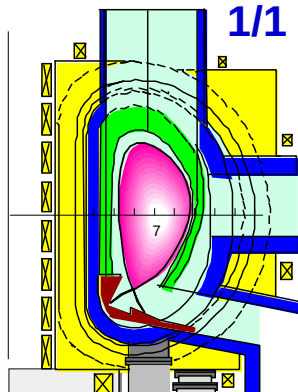
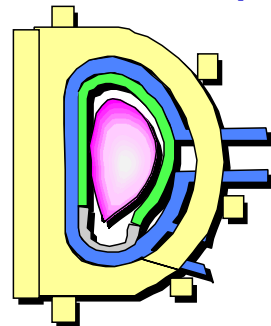
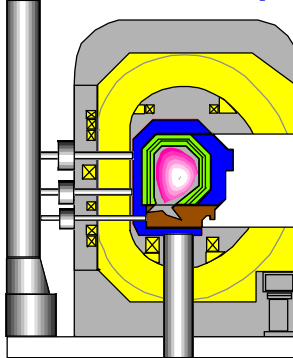
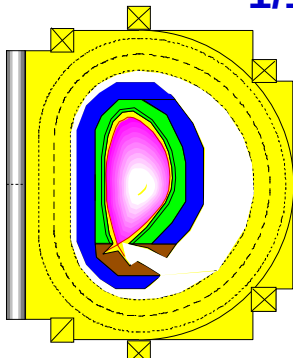
Setup of Power Core Components





Tokamak Reactor Design in JAERI

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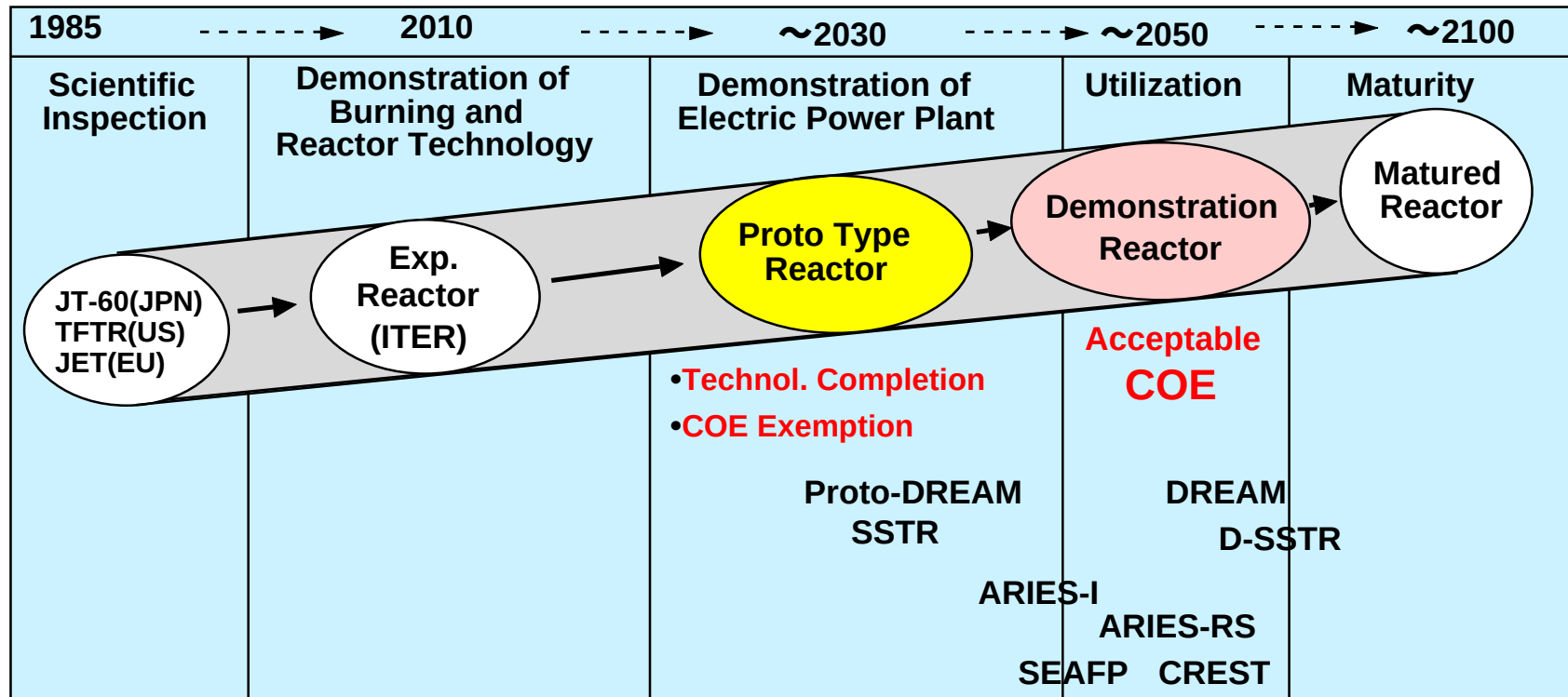
	SSTR (1990)	A-SSTR (1996)	DREAM (1996)	D-SSTR (1999)
				
※ : Remote radiative cooling is fully expected.		Needs Pull Sketch		
Type Plasma current I_p Major radius R_p Aspect ratio A Toroidal field B_t Max. neutron load f_n Blanket heat flux q_w Div. heat flux q_{div} Neutron fluence F Max. coolant temp. T_{max} Fusion power P_f Current drive P_{CD} Blanket Mat. Coolant Bulk Shield Mat.	DEMO 12MA 7m 4 9T 5MW/m ² 1MW/m ² 7MW/m ² 7MWa/m ² 550°C 3GW 60MW F82H P. Water F82H	Commercial 12MA 6m 4 11T 10MW/m ² 2MW/m ² 4MW/m ² ※ 14MWa/m ² 650°C 4.5GW 60MW F82H P. Water F82H	Commercial 9.2MA 16m 8 14.5T 4MW/m ² 0.5MW/m ² 7MW/m ² 10MWa/m ² 900°C 5.5GW 50MW SiC/SiC He SiC/SiC, TiH ₂	Commercial 12MA 6.2m 4 11T 8MW/m ² 2MW/m ² 4MW/m ² ※ 12MWa/m ² 900°C 4.5GW 60MW SiC/SiC He TiH ₂

Major Milestones on Road to Fusion Power Reactor

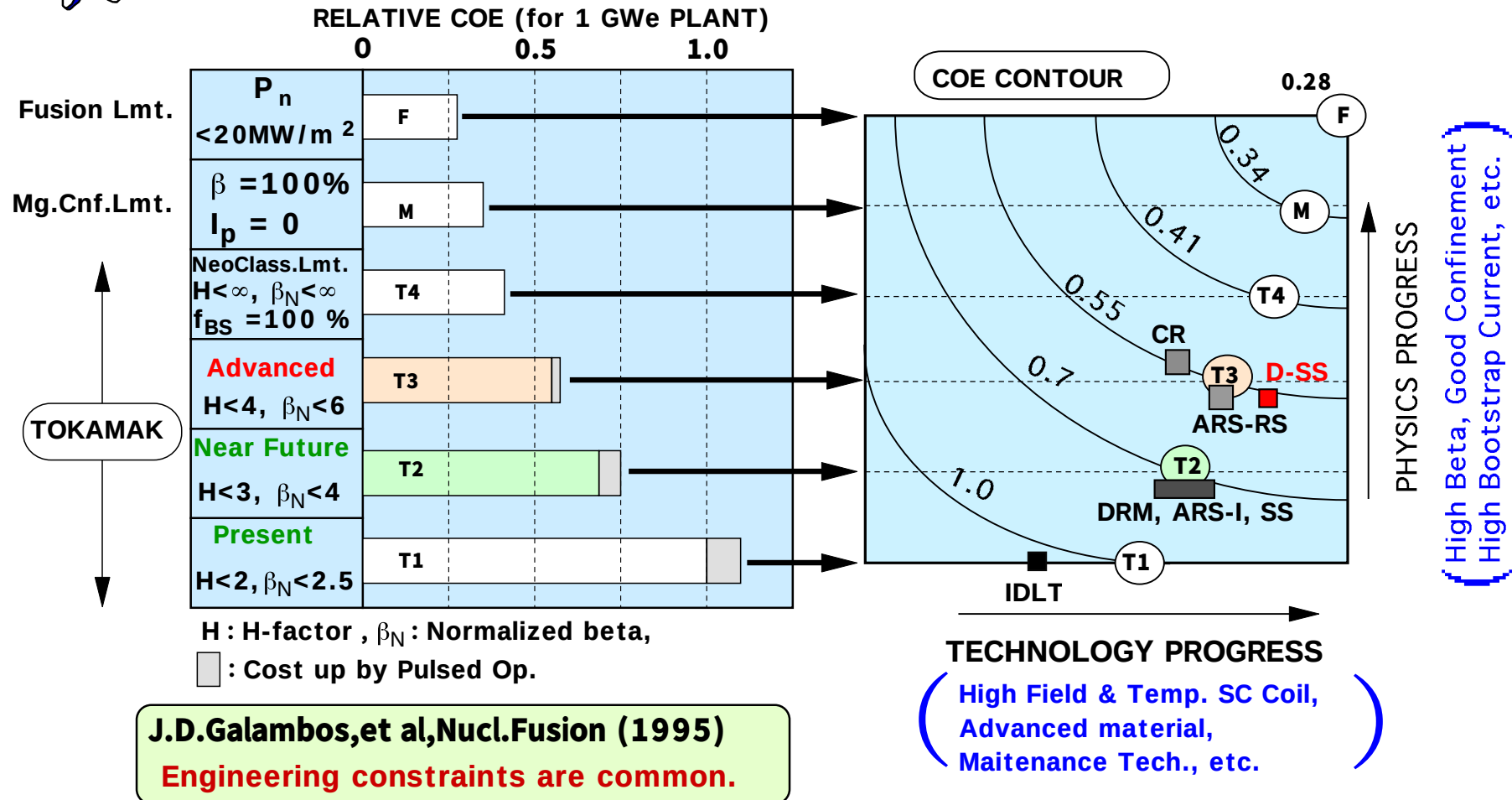
- 4 -



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COE DEPENDENCE ON PHYSICS CONSTRAINT FOR D-T FUSION



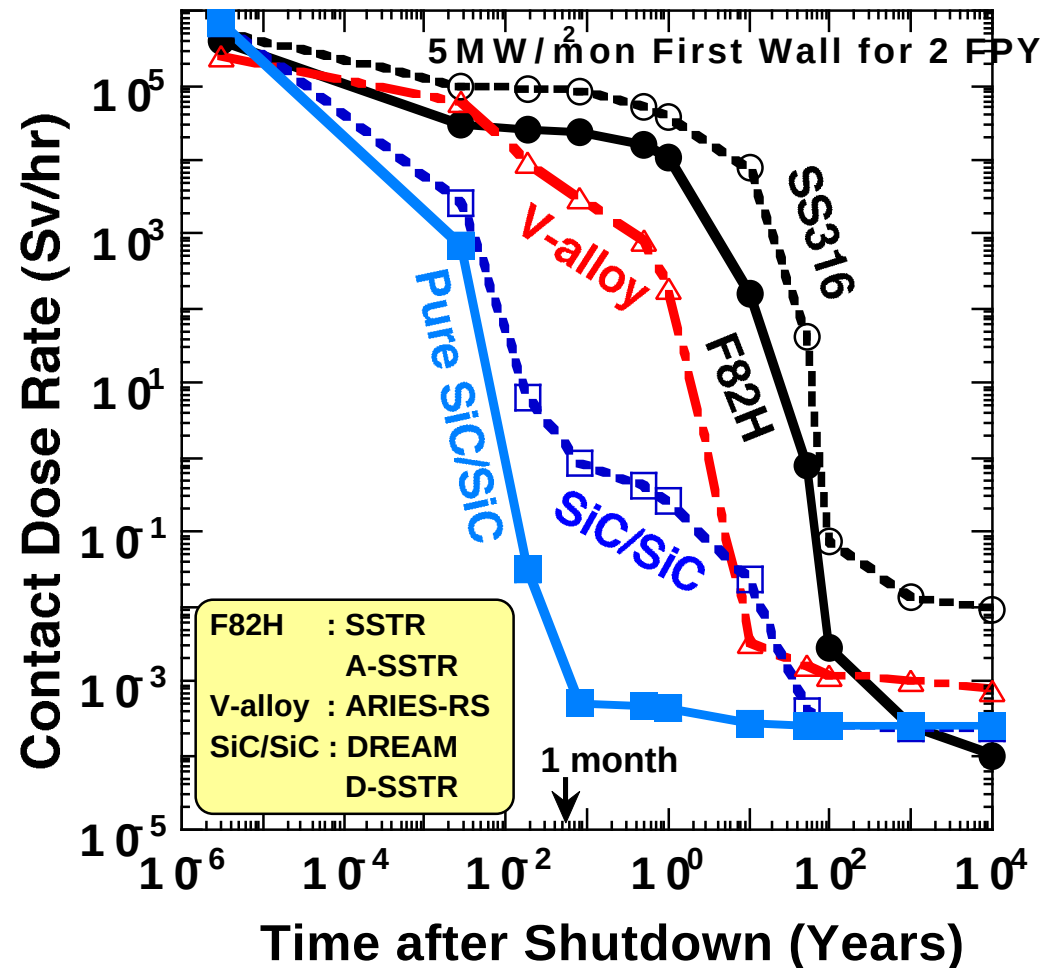
Cost Competitiveness of Fusion is not Promising.

Decline Comparison of Activated Materials

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D-SSTR

- SiC/SiC Weight of Replaceable Blanket is 125 Ton.
- Every 2 years Replacement and 30 years Life time.

Total Radwaste is 1900 Ton.

After Irradiation of 10MWa/m²

Induced Activity

10¹⁸ Bq/ton for SS, F82H

5x10¹⁵ Bq/ton for SiC/SiC

Total Radio Activity

• F82H : 7.5x10²⁰ Bq (2.0x10¹⁰ Ci)

• SiC/SiC : 1.5x10¹⁸ Bq (4.0x10⁷ Ci)

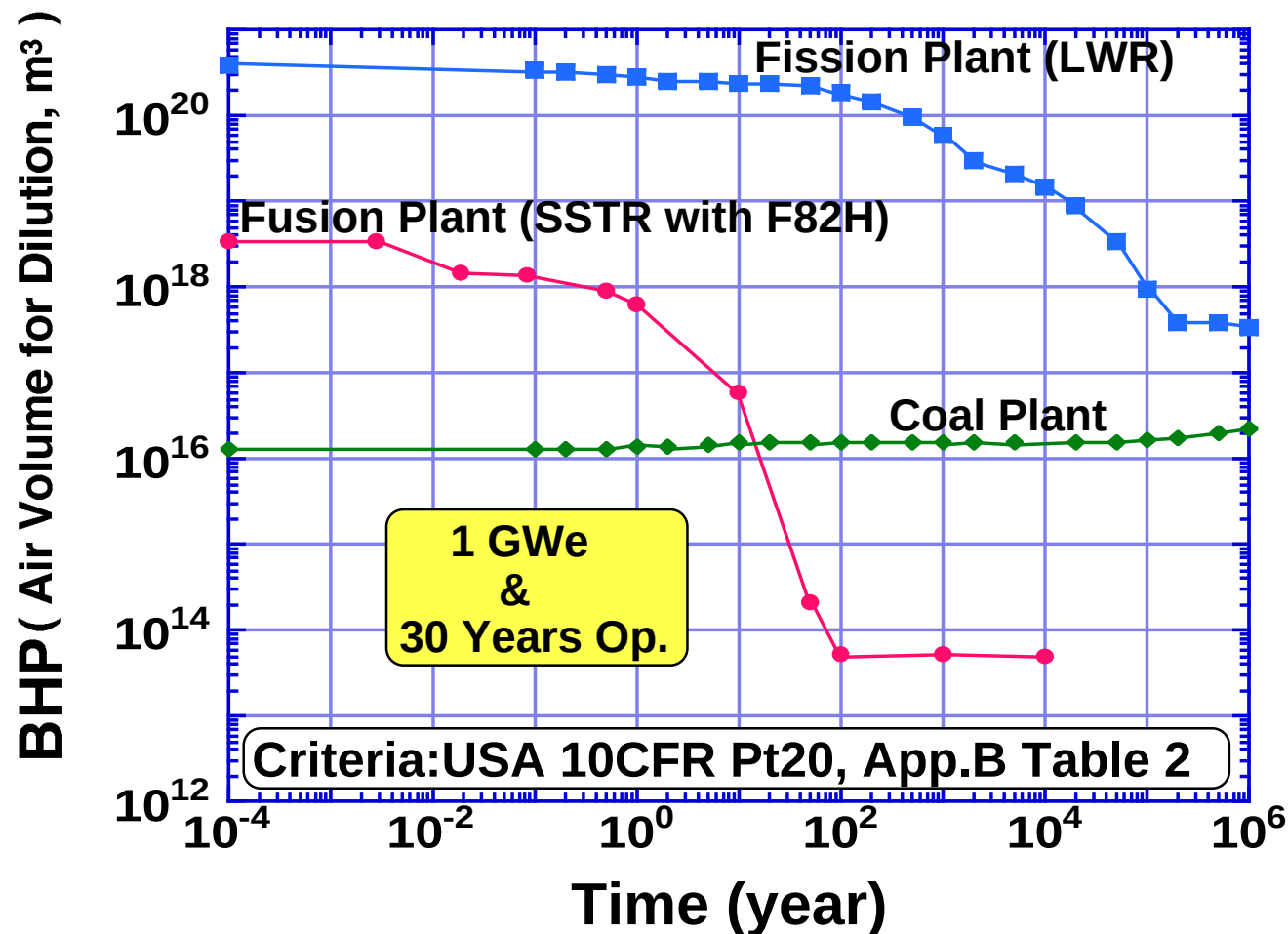
Dose Rate Rapid Decline of Pure SiC/SiC : < 1mSv/h for 1 month cooling

Biological Hazard Potential

(Fission, Fusion and Coal)



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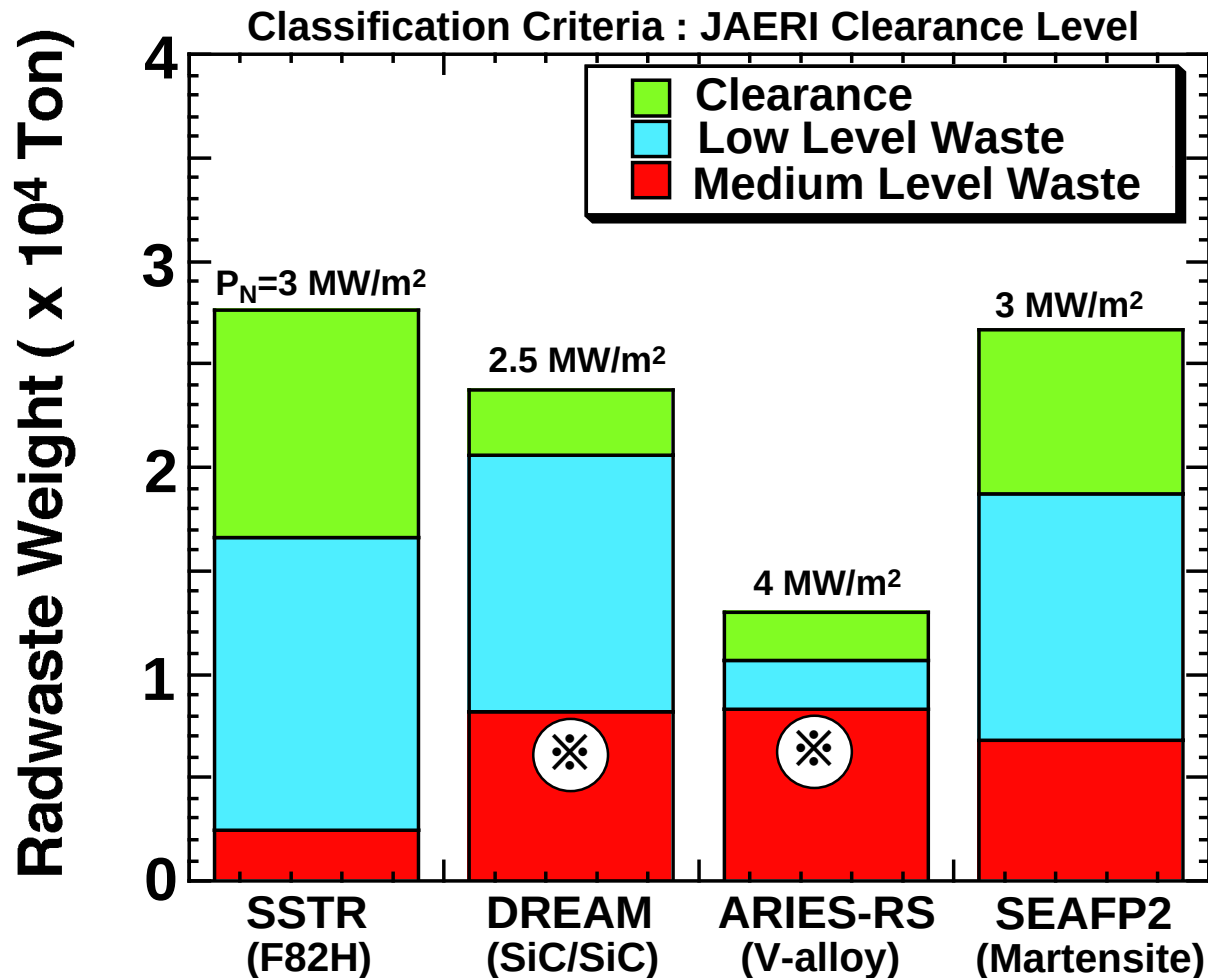
Even the F82H fusion plant can catch up with the coal plant within 15 years.
BHP of a SiC/SiC fusion plant may be negligible.

Radwaste Weight of Tokamak Reactor



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Medium level waste requires 30 years care before the burial.

 is derived from impurities,
 hence
can be replaced
 by .

Material Comparison from Neutronics Viewpoint



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Material	Activation Intensity for Maintenance (for replacement)	Neutron Shielding Effectiveness (for thickness)	Radwaste Quantity after Plant Life Time		
			Total	Low Level	Medium Level
SiC/SiC	$\sim 10^{-7}$	0.2~0.3	1 (2×10^4 Ton)	60 %	40 % (N and Cl)
				100 % [*]	0 % [*]
F82H	1 (3×10^4 Sv/h)	~ 0.7	~ 0.8	85 %	15 % (Itself)
V-alloy	$\sim 10^{-1}$	~ 0.8	~ 0.65	22 %	78 % (Impurity)
TiH ₂	$10^{-3} \sim 10^{-4}$	1	~ 0.5	> 90 %	< 10 %

^{*}without impurity(N and Cl)

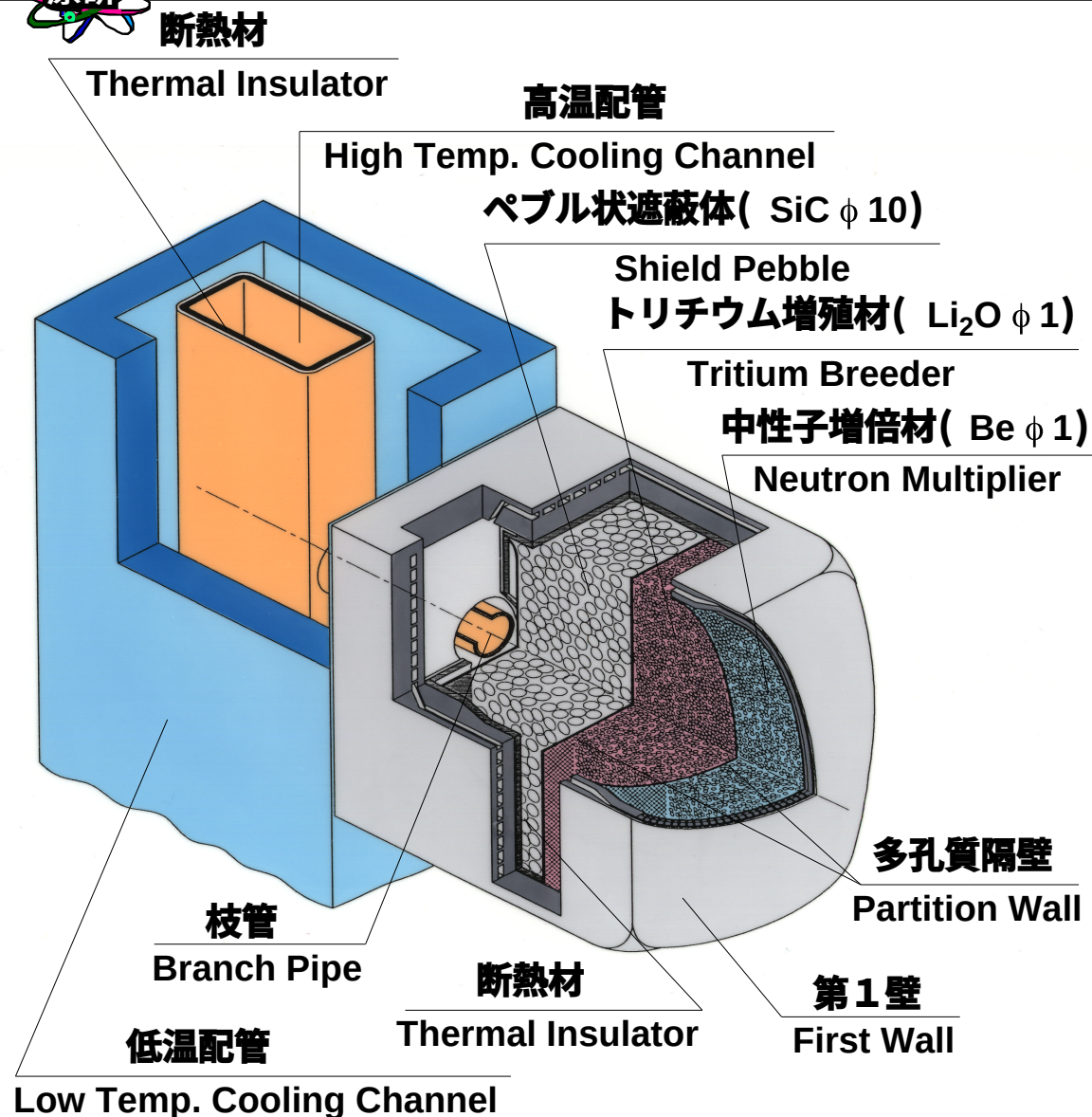
**For power core components, the combination of SiC & TiH₂ is preferable.
For conducting material, V-alloy is desirable.**

Artist's Conception of DREAM Blanket Module

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Parameters

Structural Mat. : SiC/SiC Comp.
Therm. Cond. : 15W/m/K
Vessel Size : 500x500 mm
Coolant : Helium
Coolant Pres. : 10 MPa
Coolant Temp. : 600/900 °C
Coolant Vel. : 100 m/s
Wall Load : 3 MW/m²

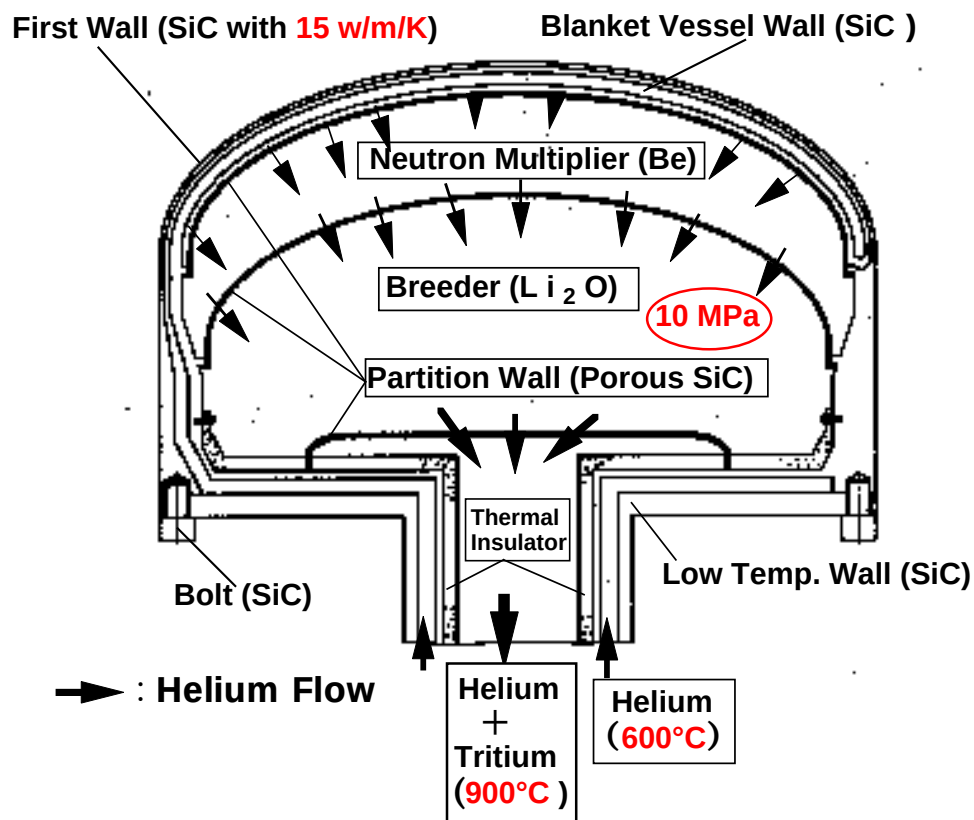
Blanket & Divertor Modules of DREAM



- 1 1 -

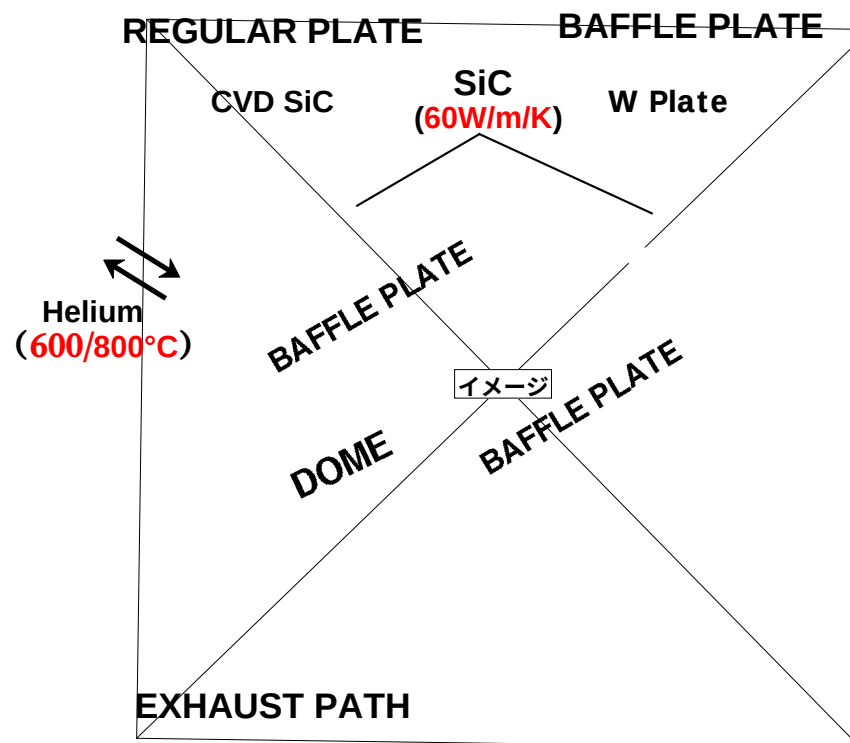
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$$P_{FW} = 0.5 \text{ MW/m}^2$$



MUSHROOM BLANKET MODULE
(Solution)

$$P_{DIV} = 7 \text{ MW/m}^2$$



DIVERTOR MODULE
(No Solution)

Manufacturing Process of Blanket Module

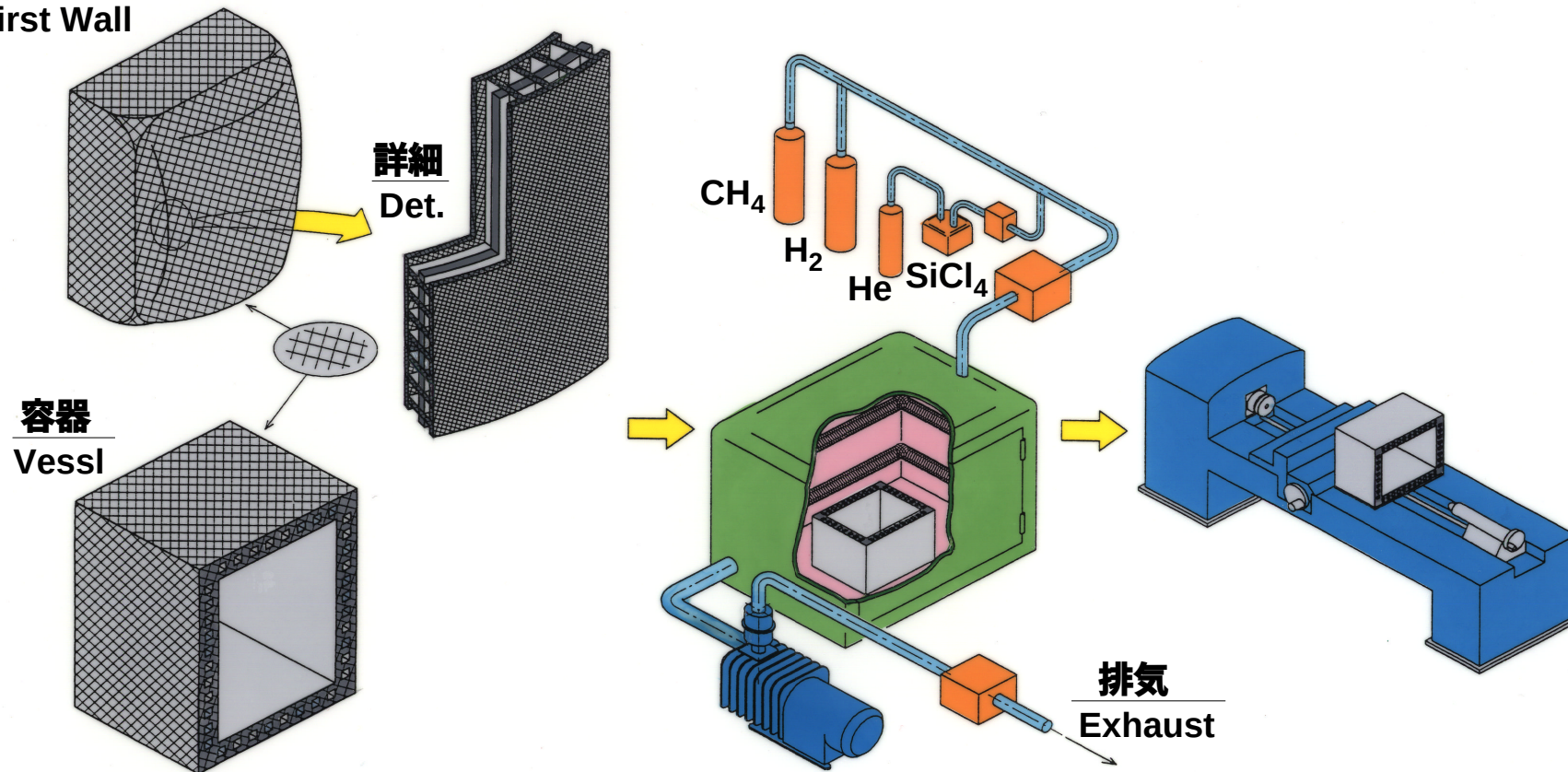
- 1 2 -



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第1壁

First Wall



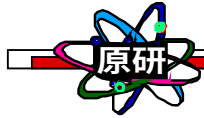
繊維織込工程
Textile Preform

含浸と高密度化
Densification

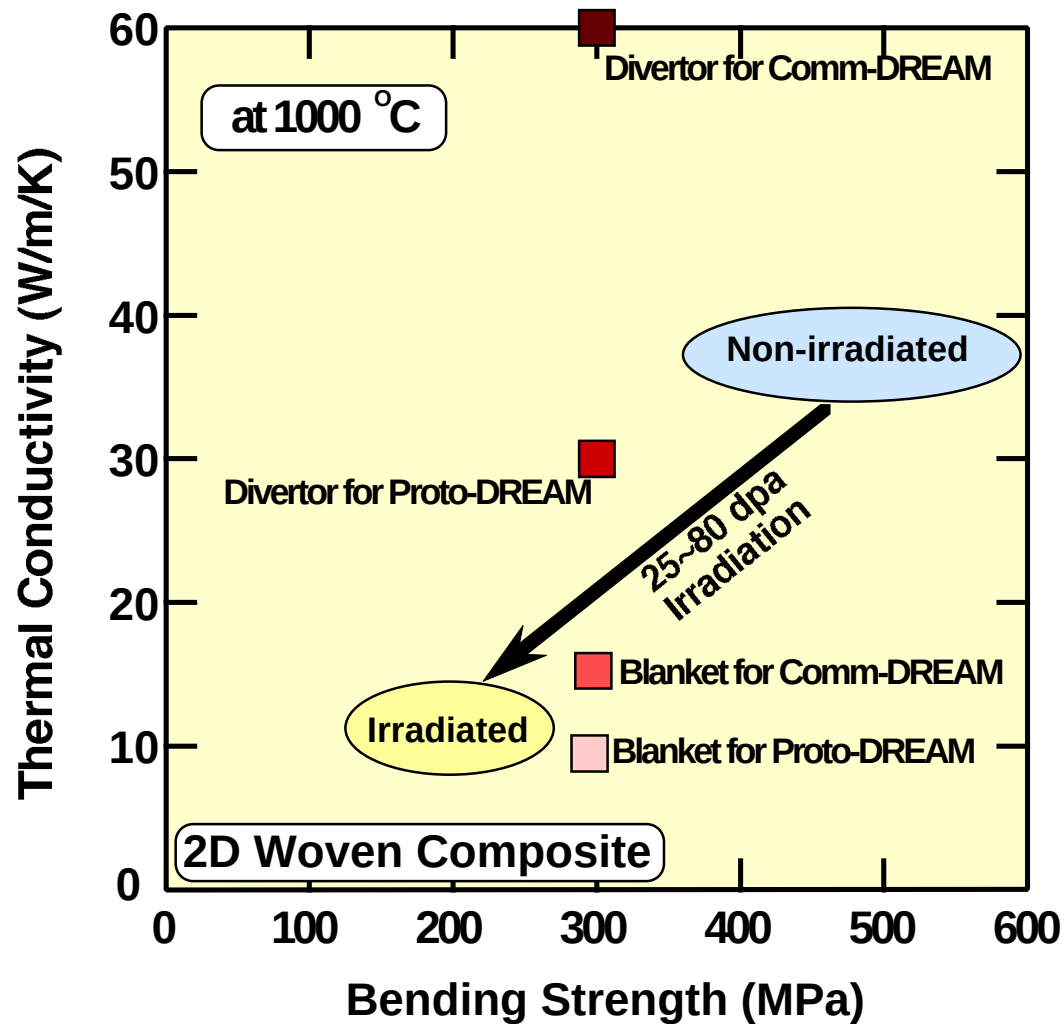
機械加工と最終仕上
Machining & Finishing

Neutron Irradiation Degradation of SiC/SiC

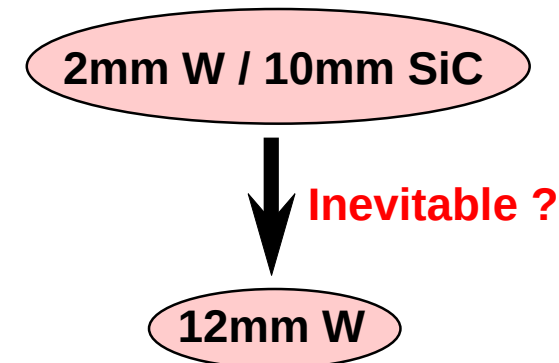
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JAERI



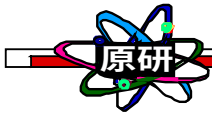
Divertor Plate of Future Reactor Requires Unrealistically high Performance to SiC/SiC Composite.



Thermal Stress on SiC/SiC

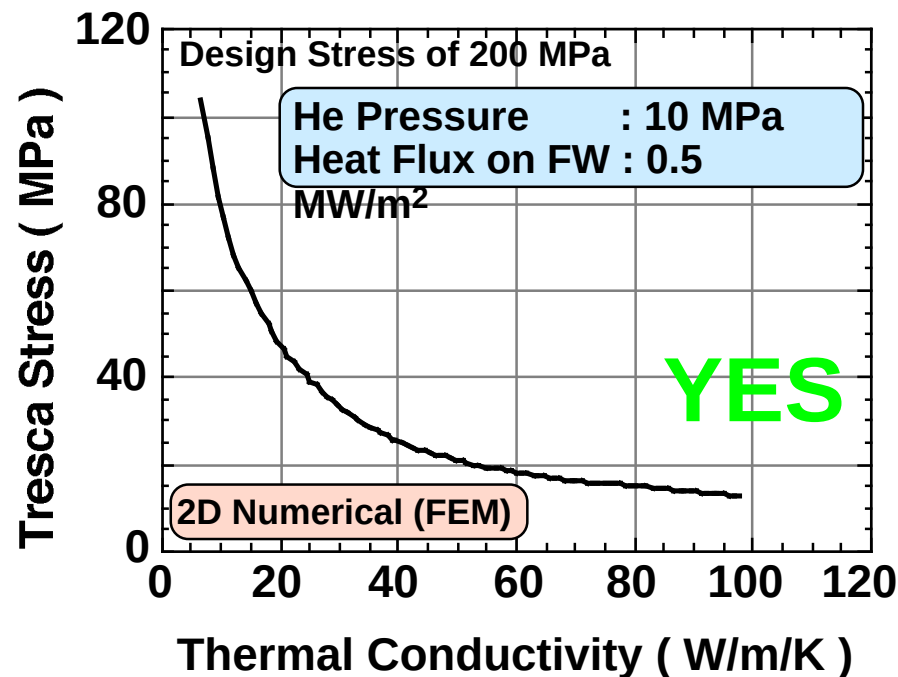
(High Heat Flux Component)

- 1 4 -

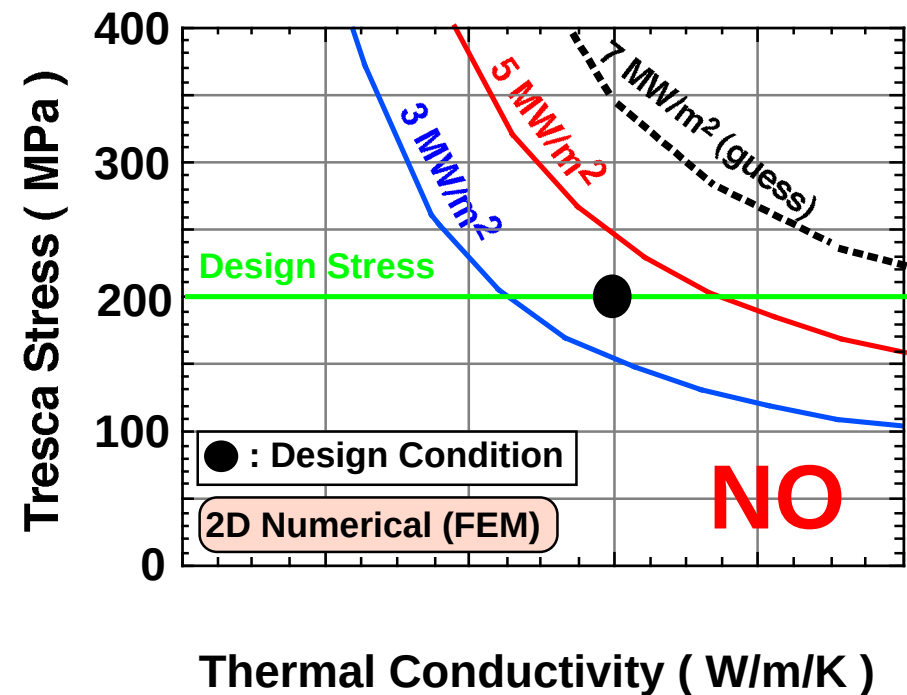


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Blanket First Wall

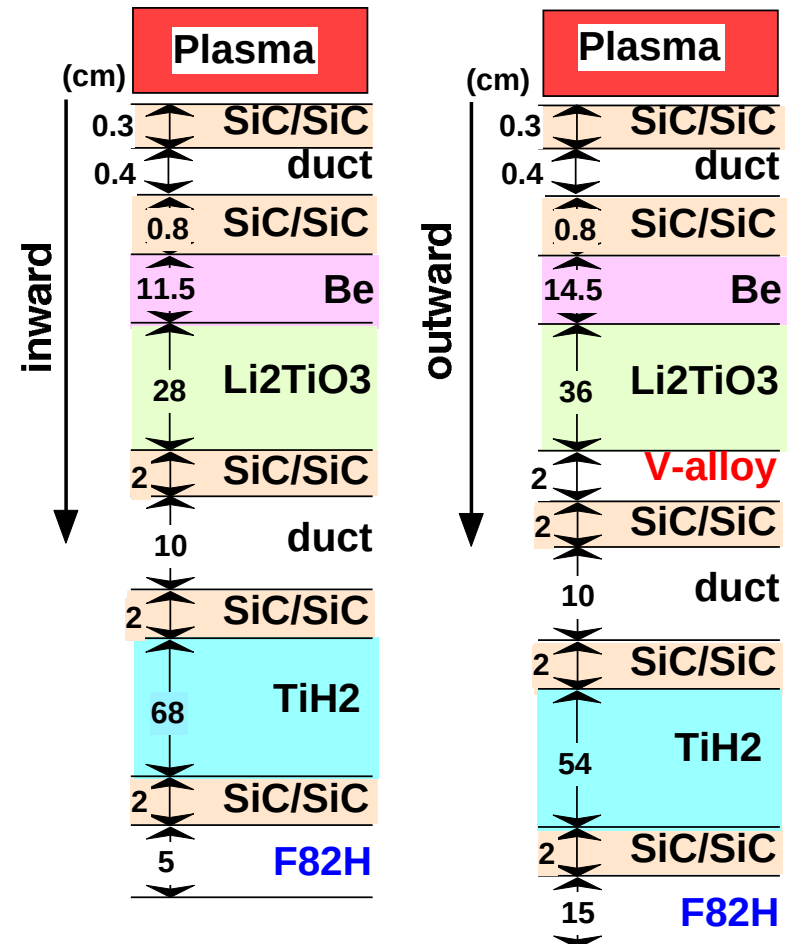
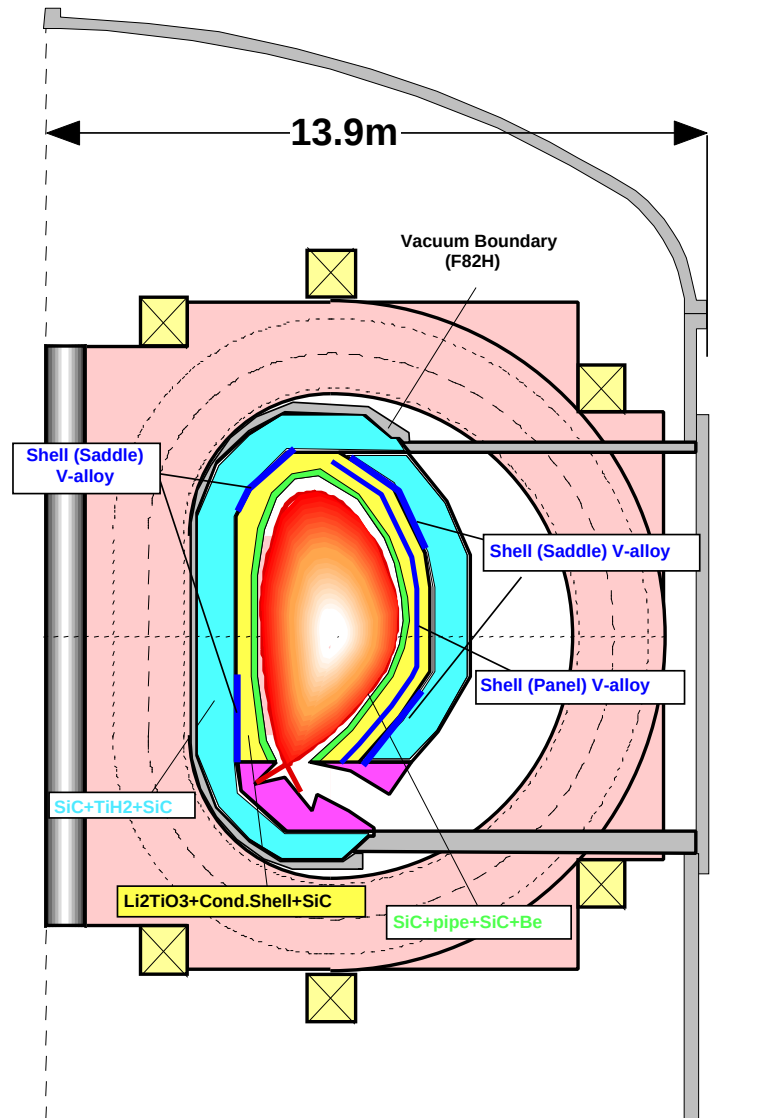


Divertor Plate



- SOLUTION OPTION {
- Full W Use for Divertor Plate
 - Full Remote Radiative Cooling in Divertor Region
 - Development of Excellent SiC/SiC

Radial Build of D-SSTR



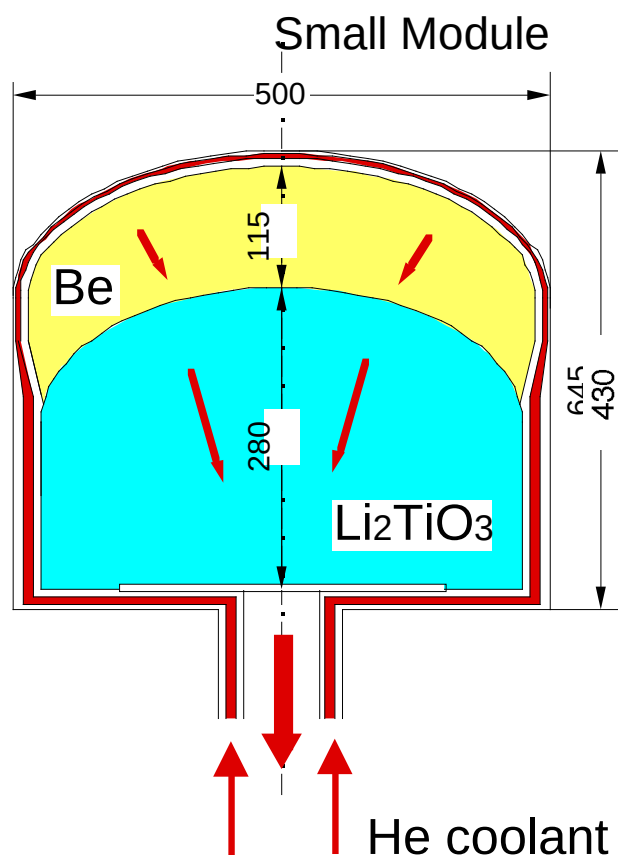
TiH₂ as Bulk Shield

Blanket Module of D-SSTR

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Structure Material : SiC/SiC Comp. (Therm. Cond. of 15W/m/K)
 Vessel Contents : 1φPebble Be and 1φPebble Li_2TiO_3
 Coolant and T Purge Gas : He (10MPa & 600°C_{IN} / 900°C_{OUT})



Small Blanket(221.69kg)

Be =0.02875m³

=53.59kg

Li_2TiO_3 =0.05509m³

=121.6kg

SiC/SiC =0.01485m³

=46.5kg

Large Blanket(301.57kg)

Be =0.03625m³

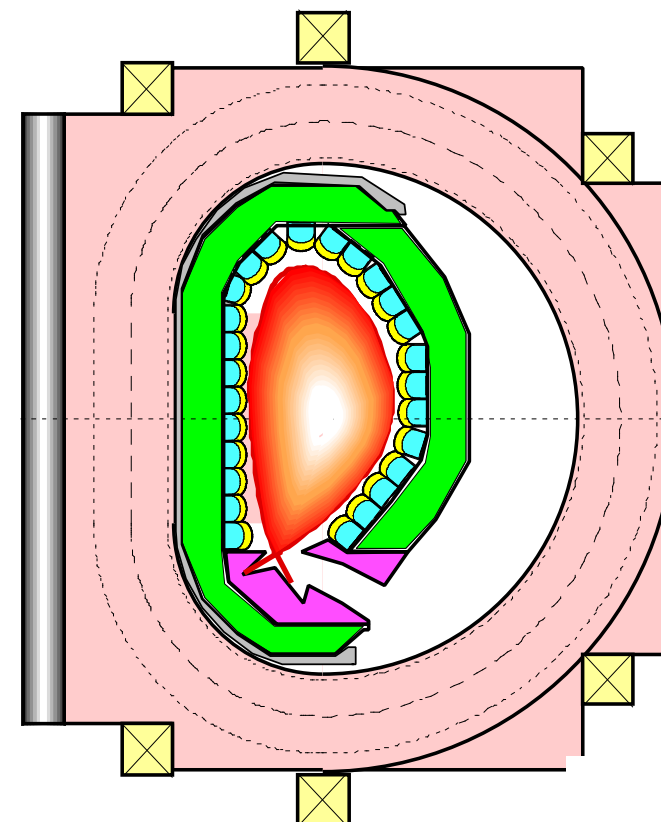
=67.57kg

Li_2TiO_3 =0.07509m³

=165.7kg

SiC/SiC =0.02182m³

=68.3kg



1950 modules S(675),L(1)

Bulk Shield Structure Filled with TiH_2

Vessel Material : SiC/SiC Comp.

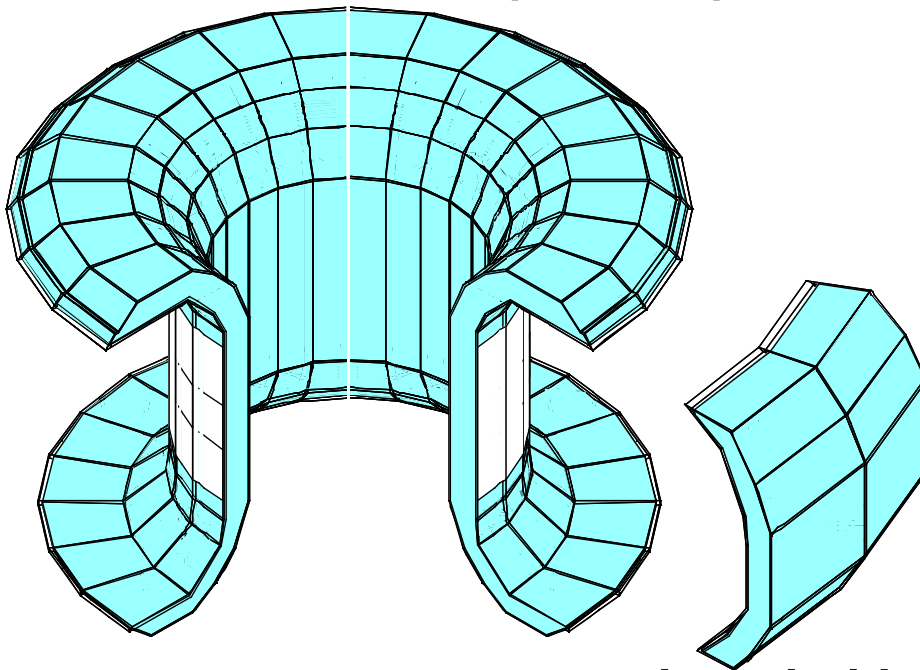
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Inboard Shield
(Permanent & Lifetime Use)

$$\phi_n^{\text{IN}} = \begin{cases} 9 \times 10^{17} \text{ m}^{-2}\text{s}^{-1} (> 0.1\text{MeV}) \\ 2 \times 10^{16} \text{ m}^{-2}\text{s}^{-1} (14\text{MeV}) \end{cases}$$



Outboard Shield
(Replaceable but Lifetime Use)

$$= \begin{cases} 5 \times 10^{17} \text{ m}^{-2}\text{s}^{-1} (> 0.1\text{MeV}) \\ 1 \times 10^{16} \text{ m}^{-2}\text{s}^{-1} (14\text{MeV}) \end{cases}$$

Shielding effectiveness of TiH_2
is
more superior than SiC/SiC by
several times.

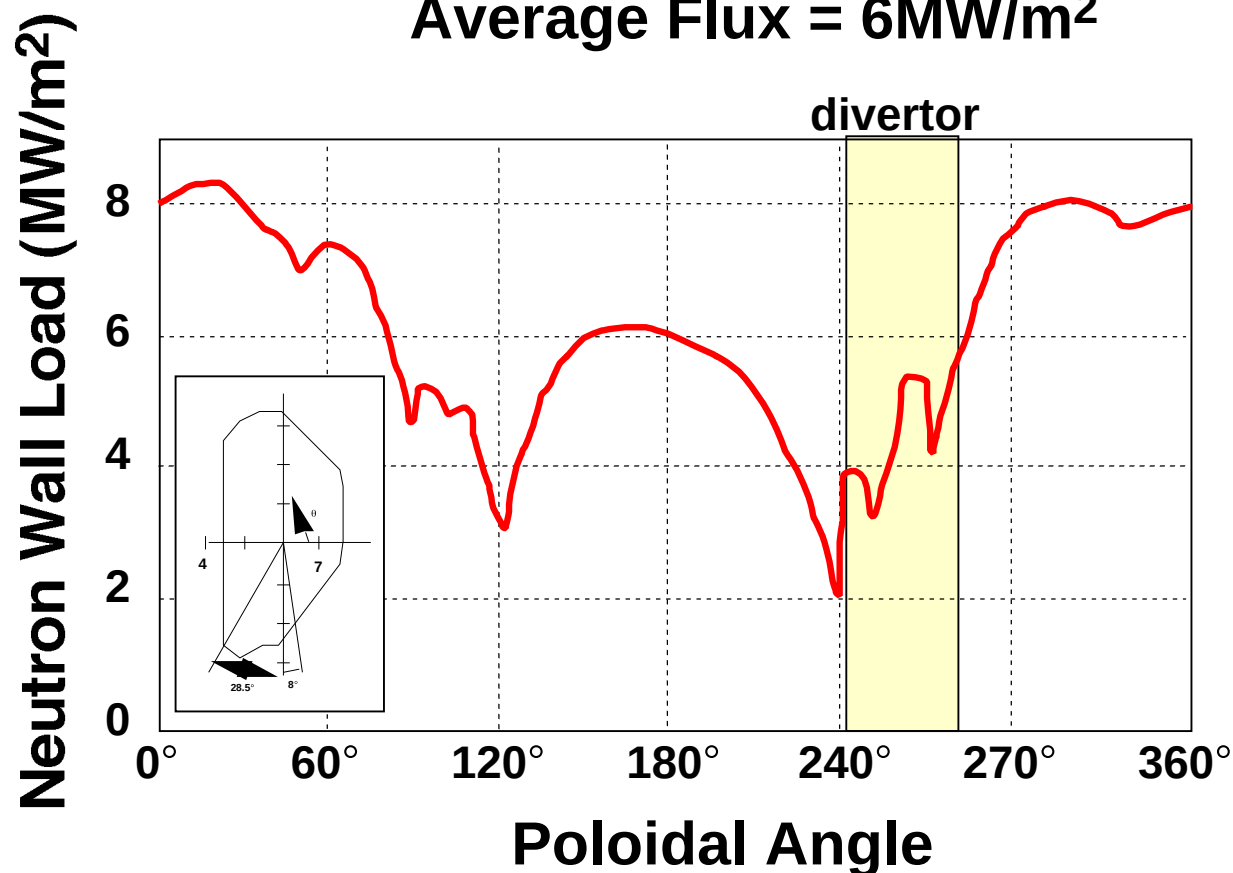


Neutron Wall Load in D-SSTR

D-SSTR : Compact and high power reactor
⇒ Very high neutron wall load

Max. Flux = 8MW/m²

Average Flux = 6MW/m²



2 years Replacement

75% Availability



**Max. Fluence
12MWa/m²**

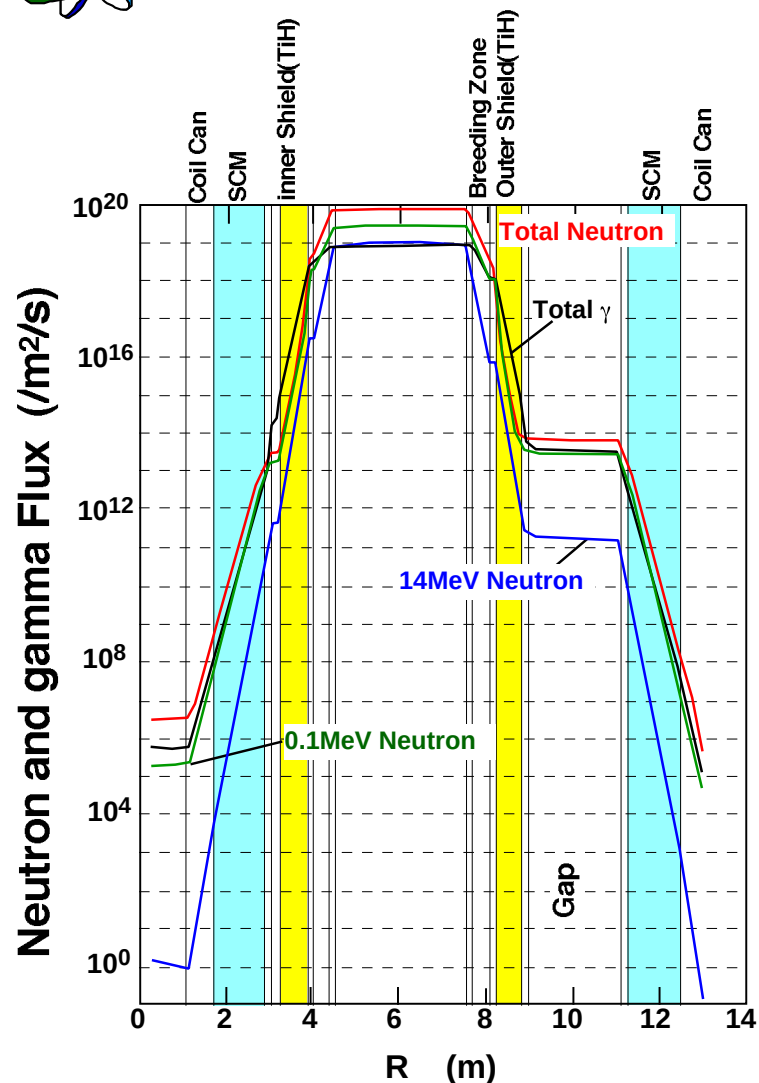
Radiation Shielding of SiC & TiH₂ Power Core

(D-SSTR Power Core Structure)

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TiH₂ for High Shielding Effect

1.35m : from First Wall to SCM
(2.5m for DREAM)

at SCM

Neutron flux (E>0.1MeV)

⇒0.9x10¹³ n/m²/s(inside)

⇒1.0x10¹³ n/m²/s(outside)

after 22.5FPY

Neutron fluence (E>0.1MeV)

⇒0.64x10²² n/m²(inside)

⇒0.71x10²² n/m²(outside)

Max. Nuclear Heating

⇒0.06 mW/cm³(inside)

⇒0.04 mW/cm³(outside)

Enough Shielding can be expected
in compact and high power reactor.

Shell Structure for Vertical Stability

5cm thickness of V-alloy Saddle Loop

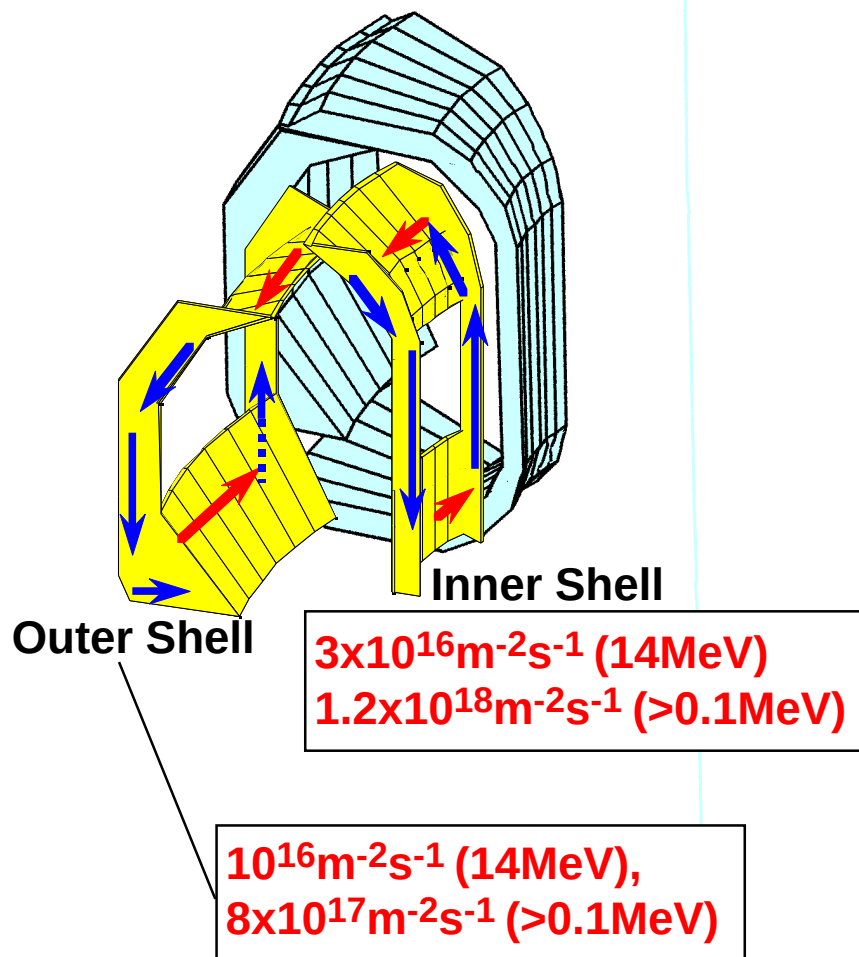
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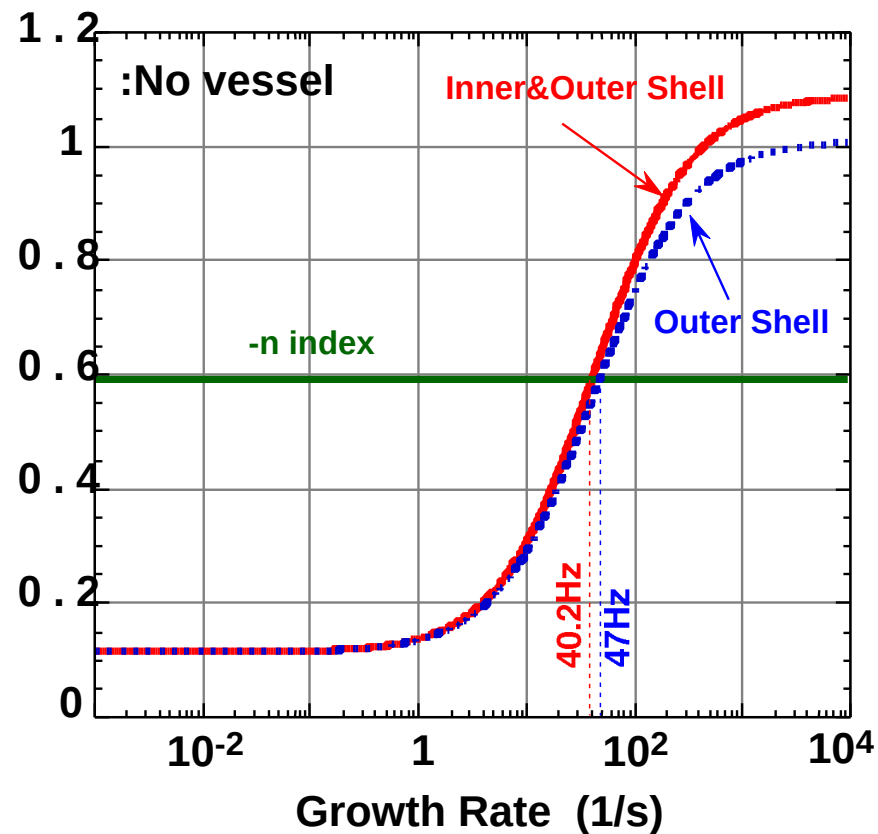


Growth rate : 40Hz

: controllable by normal conductors outside vessel

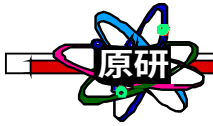


Stabilizing Effect N(s)

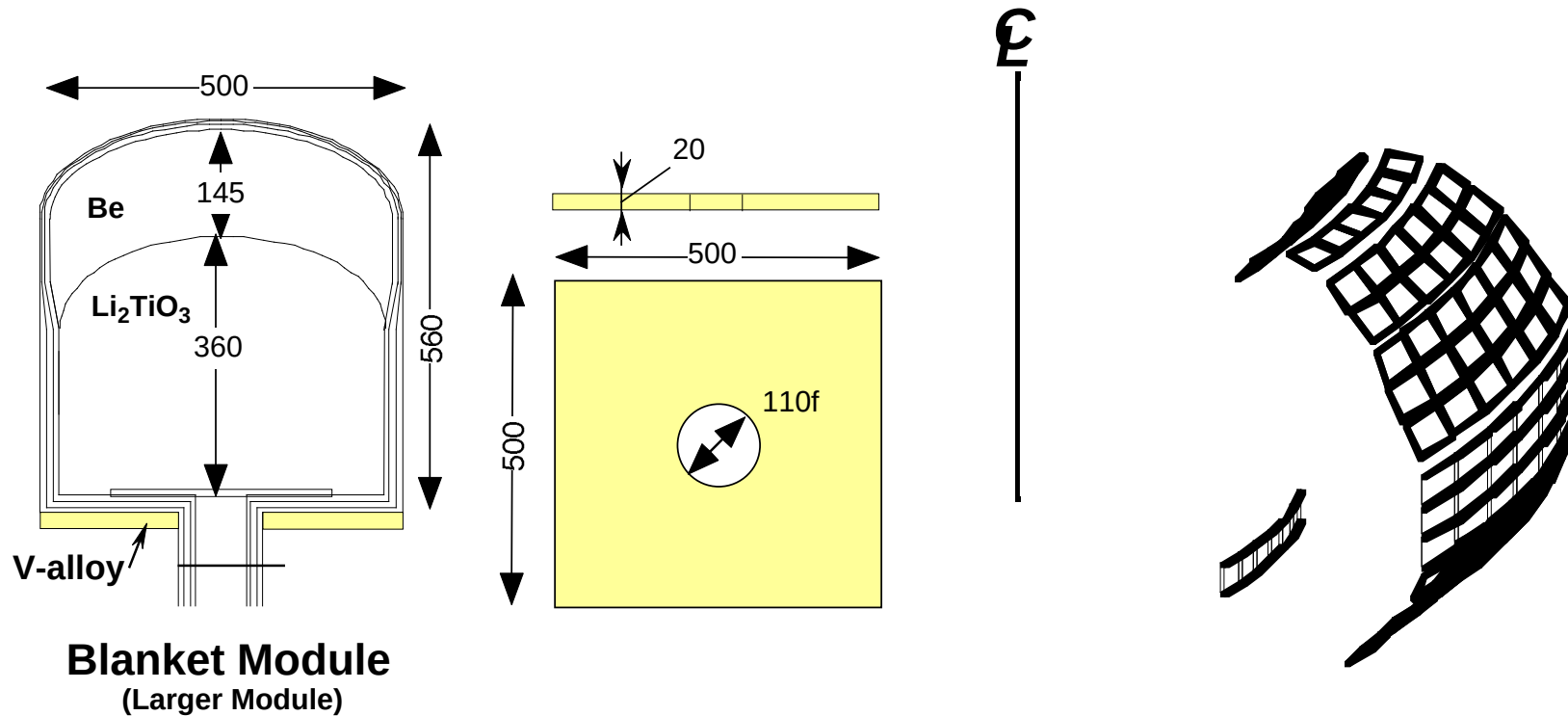


Plasma elongation 1.8 can be accepted.

Shell Structure for High β Stability



- 2 1 -
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V-alloy with 46cm x 46cm x 2cm and Hole for He Gas Coolant

**Neutron Flux: $2 \times 10^{16} \text{m}^{-2} \text{s}^{-1}$ (14MeV), $1 \times 10^{18} \text{m}^{-2} \text{s}^{-1}$ ($>0.1 \text{MeV}$)
 $4 \times 10^{18} \text{m}^{-2} \text{s}^{-1}$ (Total)**

Summary



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Material use optimization for
fusion power core components
has been attempted in
D-SSTR.

- **SiC/SiC for Replaceable Blanket Structure Material**
- **TiH₂ for Bulk Shielding material**
- **V-alloy for Conducting Material**
- **W for Divertor Plate**