



DOE OFES/DP

The Strength of Solid DT

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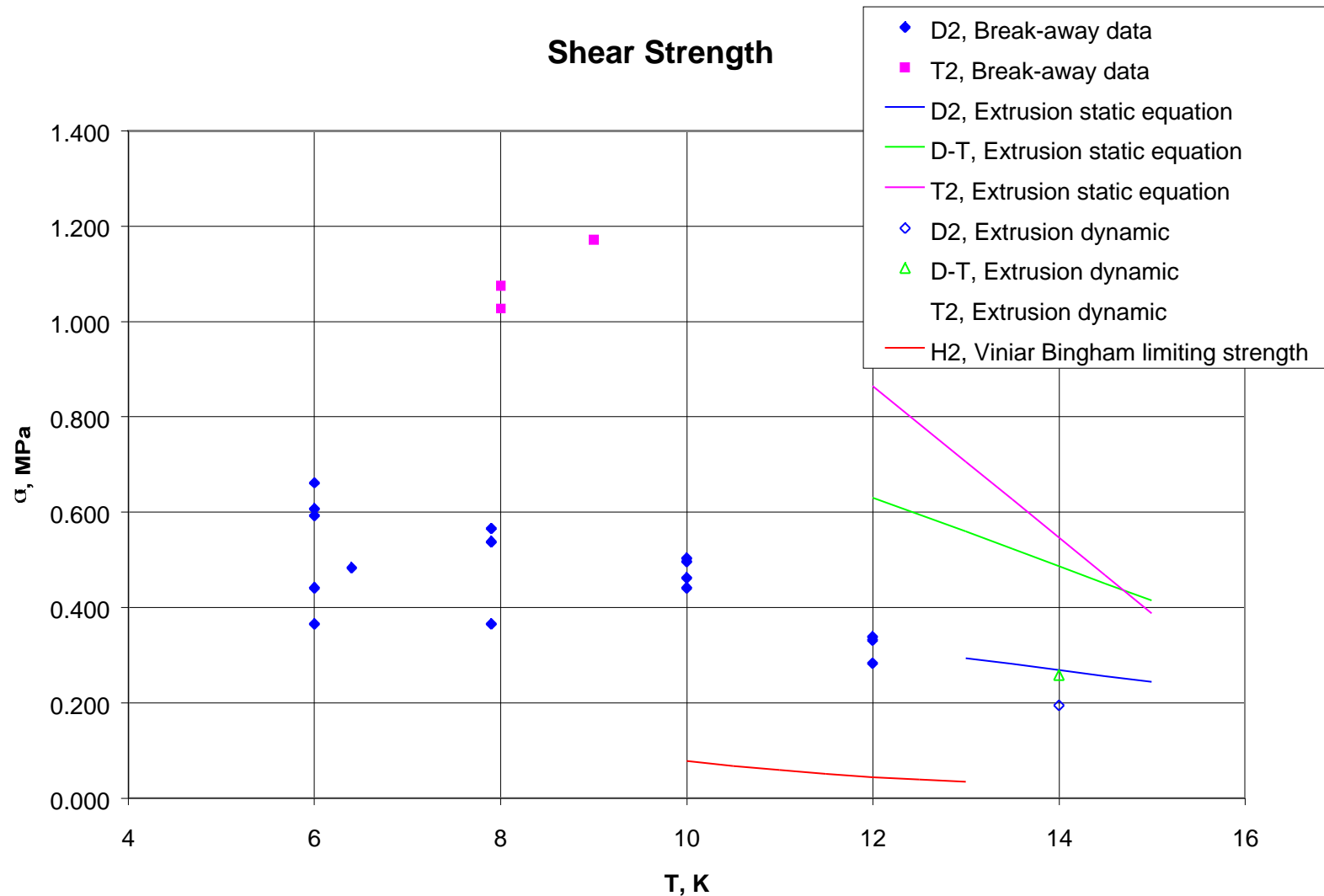


Summary of literature data on solid hydrogens

- For solid H₂: high pressure data @ 4.2 K (Towle '63)
- For solid D₂: Stress vs. strain & Young's modulus on polycrystalline samples (~ 10 mm dia.) from 1.4 K to 15.6 K (Bol'shutkin et al. '70)
 - Souers' evaluation of this data suggests that at 16.4 K (n.b.: 2.4 K below the triple point) - the yield stress 50 kPa.
- For T₂ and DT, ONRL data on pellet extrusions gives shear strength estimates of ~800 to 400 kPa from 12 K to 15K, resp. The data extrapolates to ~ zero at the triple points. (Gouge '99)
- For 50-50 DT near the triple point: NADA!!
 - Extrapolating the Russian data to 0.8 K below the triple point, (19 K for DT), I 'guesstimate' the yield stress 10 kPa.



Hydrogenic solid shear strength data from ORNL H, D, T pellet experiments





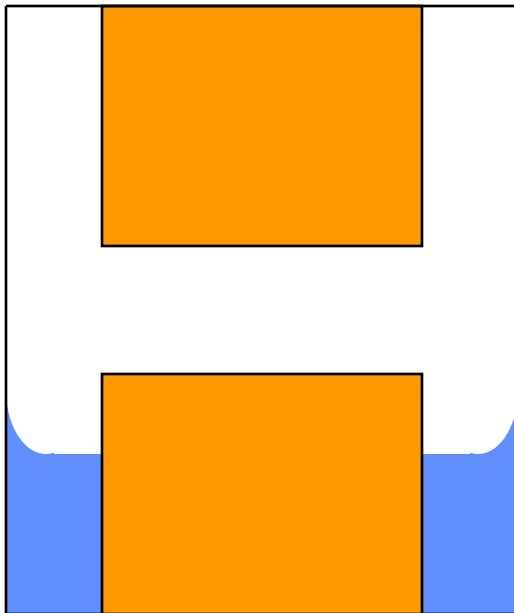
Experimental determination of the yield strength of a solid requires:

- A properly configured solid specimen (a compression specimen or a tensile stress specimen), and
- One or both of the two following methods:
 - Method A:
 - A means of applying stress
 - tensile or compressive force
 - A measurement of strain
 - a change in sample length, e.g., measured optically
 - Method B:
 - A means of applying strain
 - tension or compression from a linear actuator
 - A means of measuring the stress in the sample
 - a linear force sensor, i.e., a piezoelectric sensor

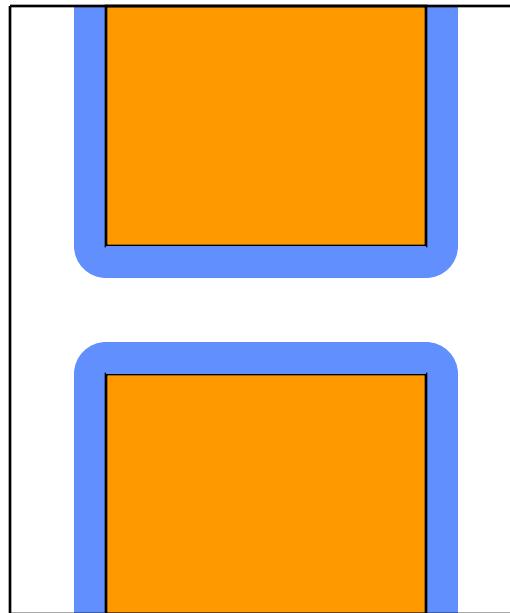


For solid DT, beta-layering permits us to fabricate a specimen for either compression or tension:

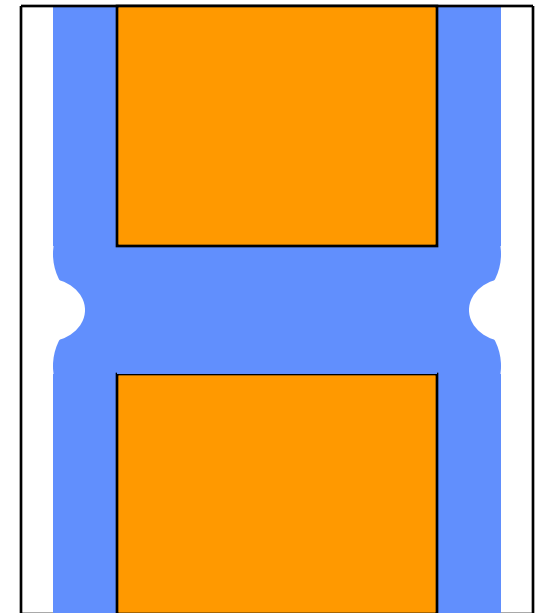
We begin with two blocks of copper, confined inside a cell at ~ 20.0 K. We then condense in an amount of liquid DT:



If we now freeze the DT and wait for beta-layering to develop a uniform solid layer at 19 K, the boundary of the layer will follow an isotherm:



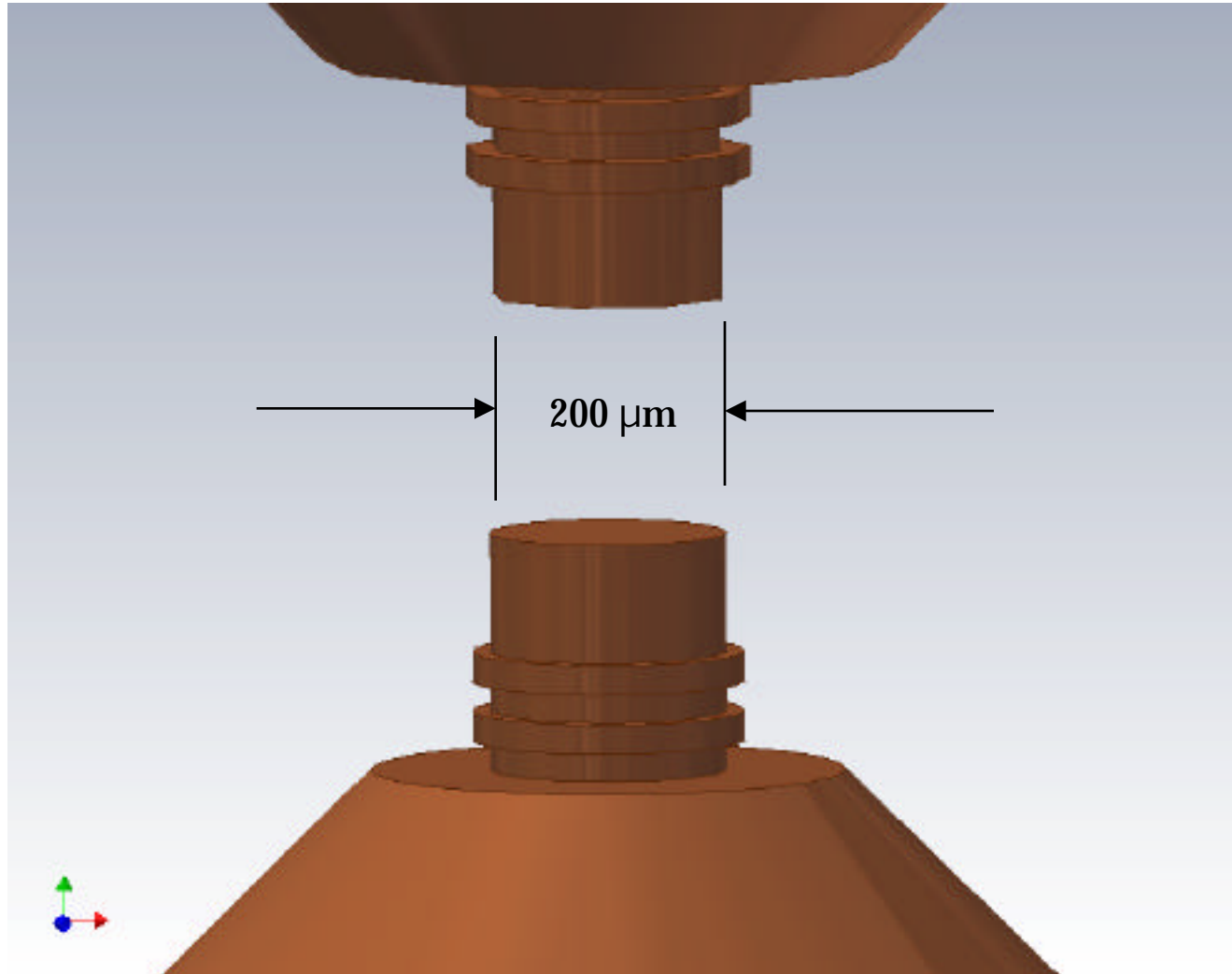
If we had added more DT, the solid would bridge the gap, creating the desired free standing specimen, complete with a notch:



Now, if we could just *move* one of these copper blocks,

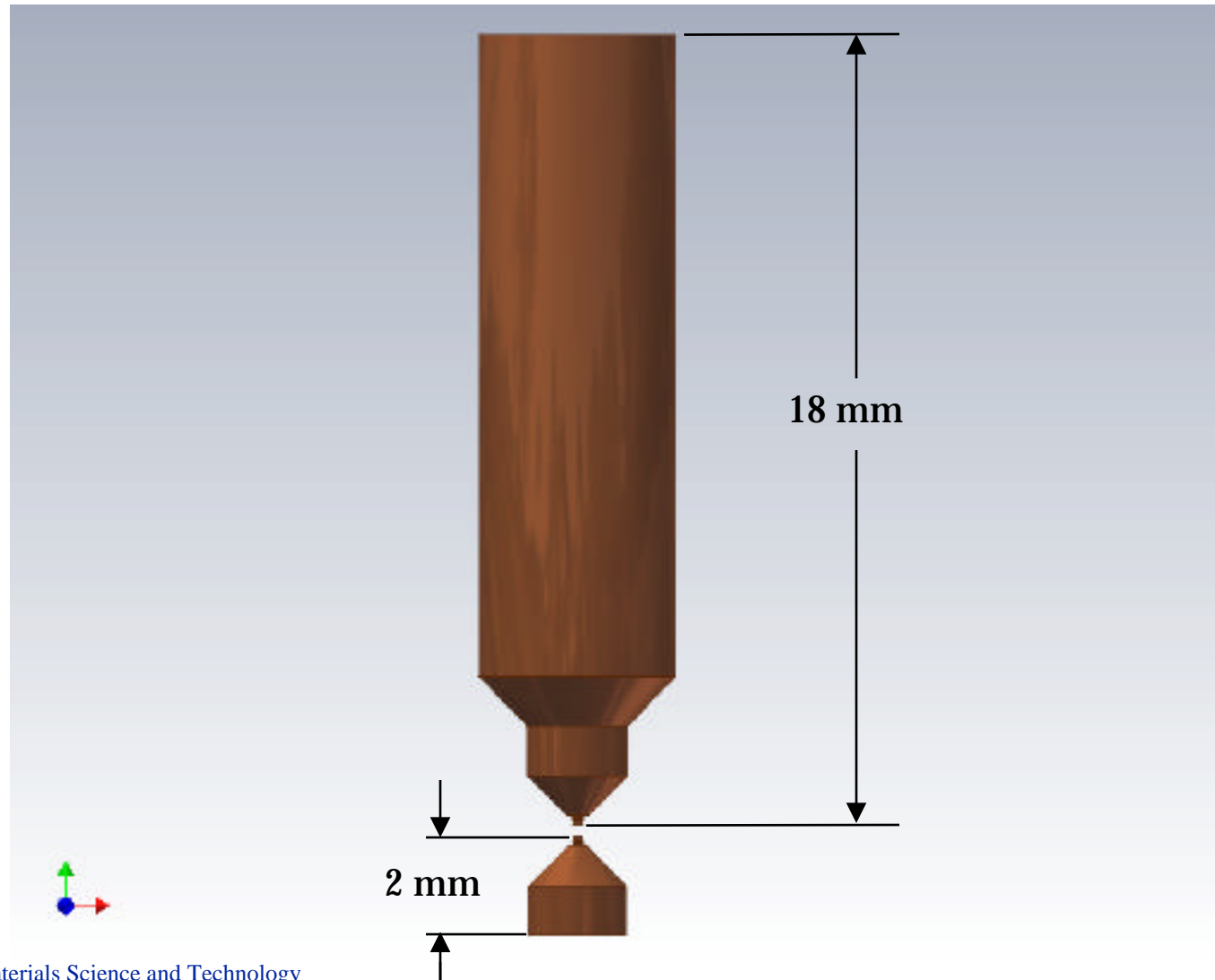


**We add some grooves to these
'sample mounting posts' to help hold
on to the solid DT specimen:**





The 'posts' are only $200\ \mu\text{m}\ \varnothing \times 200\ \mu\text{m}$ long, machined on to more manageable copper pieces:



The upper post screws onto a linear actuator, designed especially for motion at cryogenic temperatures (if we can find one!!)



At this point, I needed to seek expertise to assist in the design of a proper actuation/detection system:

As luck would have it, we have a new (Director's funded) postdoc in our division with experience in small scale materials strength measurements:

J. Gregory Swadener

Education

1998	Ph.D. Engineering Mechanics, The University of Texas at Austin Dissertation: Primary fracture toughness of a glass/epoxy interface Dissertation advisor: Kenneth M. Liechti
1992	M.S.M.E. Mechanical Engineering, University of Notre Dame
1984	B.M.E. Mechanical Engineering, Georgia Institute of Technology

Professional Appointments

April, 2001	Postdoctoral Fellow, MST-8, Los Alamos National Laboratory
1998-2001	Research Assistant Professor, University of Tennessee and Oak Ridge National Laboratory (under the direction of Dr. George M. Pharr)
1992-1998	Graduate Assistant/Postdoctoral Fellow, The University of Texas
1991-1992	Graduate Research Assistant, Notre Dame University
1988-1991	Sr. Product Engineer, Uniroyal Plastics Company
1984-1988	Analytical Engineer, Textron Marine Systems

Research Interests

Nanoindentation, interfacial fracture, adhesion, mechanics of interfaces, **small-scale mechanical behavior of materials.**



LINEAR ACTUATORS

Cryogenic motion control made easy!

Specifications:

Electronics

- *Input Power: 105-125 VAC, 2*
- *Controller Geometry: 235 x 133 x 305 mm 9.25 x 5.25 x 12 inches*
- *Control: 0-5 V analog*

Actuator

- *Stroke: 100 microns*
- *Force: 50 N ~ 11 lbf.*
- *Resolution: <0.1 microns*
- *Geometry: 10 mm dia. X 50 mm 0.394 x 2.0 inches*
- *Weight: 25 g*

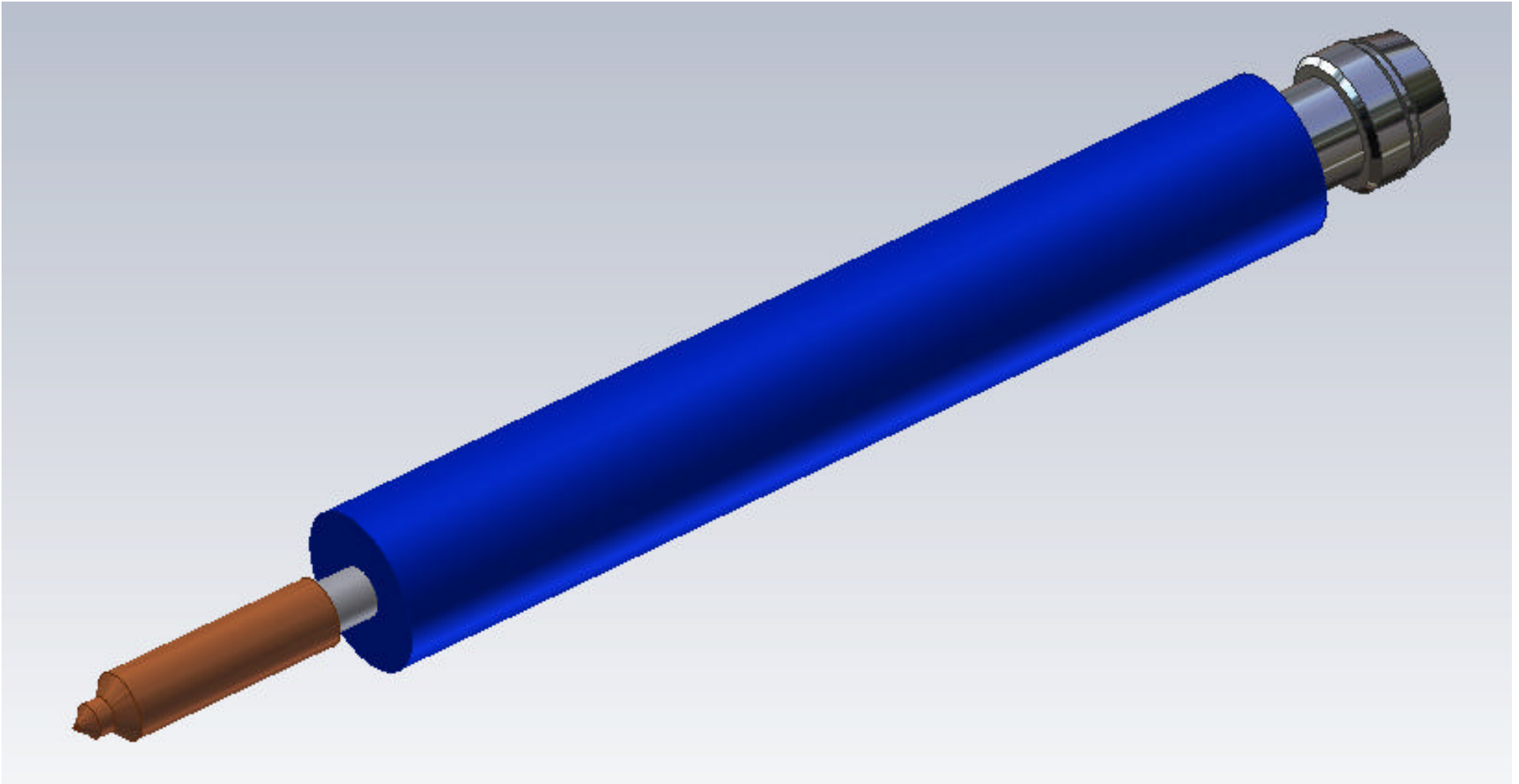


Options

- *IEEE-488.2 Interface*
- *RS232 Interface*
- *Custom cable lengths*
- *Special mounts*
- *Cryogenic operation - < 5 K*
- *Cryogenic operation - < 180 K*
- *Cryogenic electronics*
- *Custom configurations available*

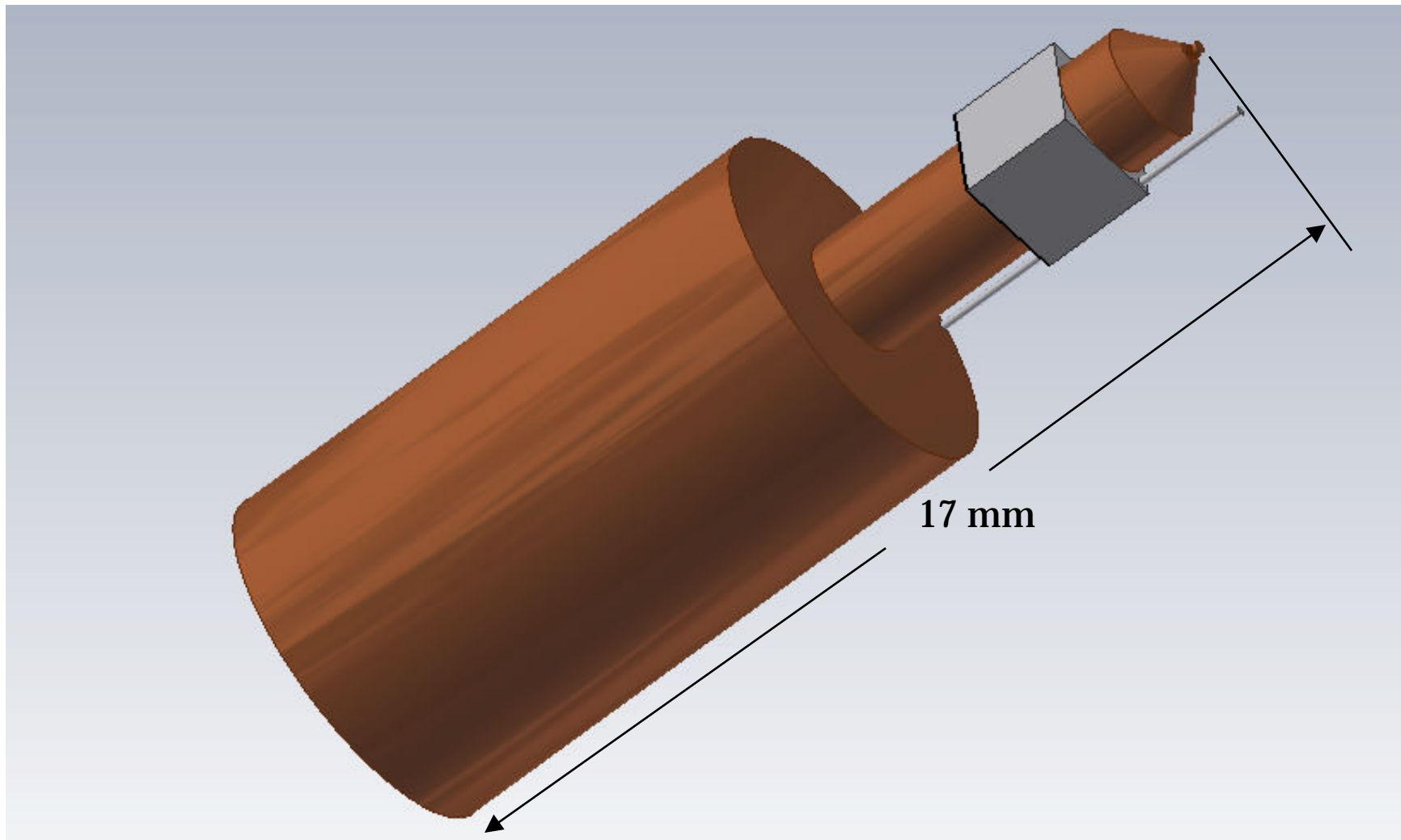


With an actuator, the upper assembly might look something like this:





We add a piezo to the lower post to measure stress:



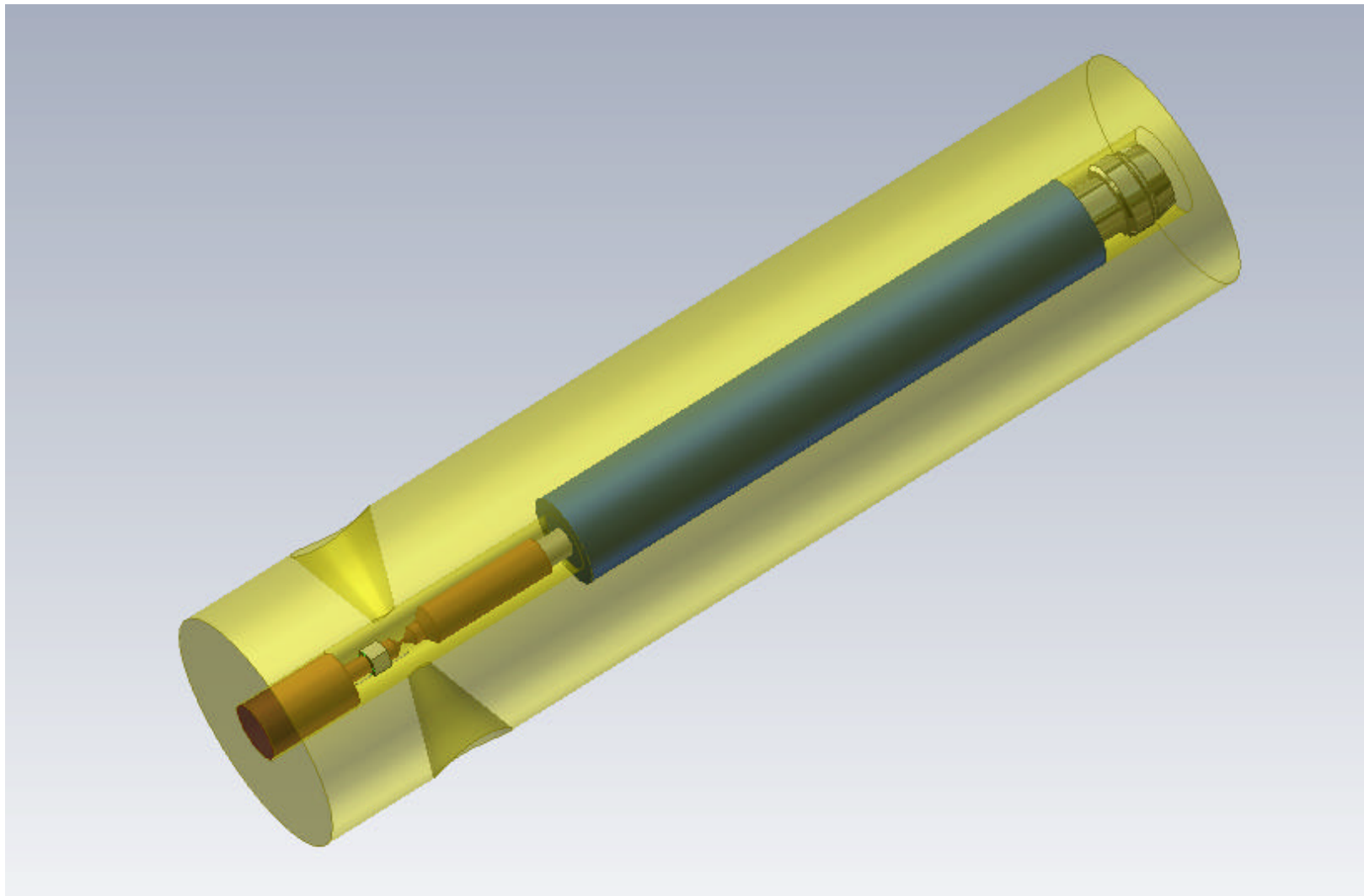


Alternatives to the piezo detector element:

Material	PCB Piezotronics	Adaptronics	Adaptronics	TRS Ceramics
	218C Charge Sensor	FPM 101	FPM 231	PZN-PT
d33 (pC/N)	n/a	200	680	2000
d31 (pC/N)	n/a	-70	-300	-950
e33/e0	n/a	600	4000	5000
Sensitivity (pC/N)	3.6			
Capacitance (pF)	14			
For 2x2x2 mm:				
Charge/Load (nC/N)	0.0036	0.200	0.680	2.000
(electron/microN)	22	1200	4100	12500
Voltage/Load (V/N)	0.26	18.4	9.6	22.6
d33 - piezoelectric constant		cf: force on piezo at yield: ~ 300 microN		
d31 - 31-piezoelectric constant				
e33/e0 - relative dielectric constant				
Note: reported values are for 295 K				
Charge and voltage sensitivity at 18 K is approximately 30%				

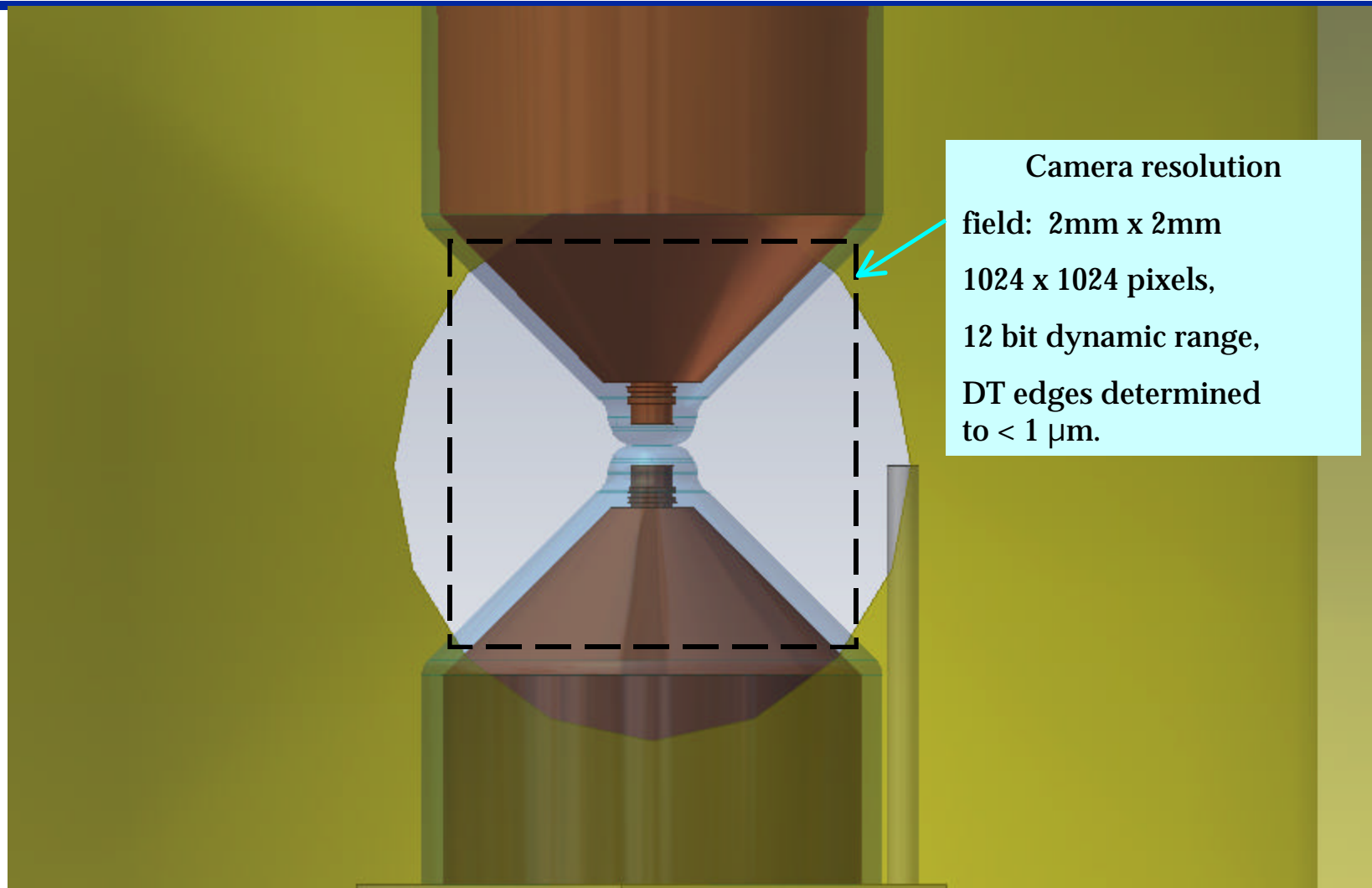


Finally, we enclose all of this assembly inside a tritium cell with optical ports:





What the camera might see:



Camera resolution
field: 2mm x 2mm
1024 x 1024 pixels,
12 bit dynamic range,
DT edges determined
to < 1 μm .



Proposed experimental procedures:

- Calibrate piezo at 19 K with 1 gram weight, then:

Assuming 1 μ N resolution,
- Run load test at 10 μ N/s
 - should resolve \sim 30 points in the elastic range
 - permits determination (with an accuracy of \sim 2-3%) of:
 - elastic modulus
 - 0.2% offset yield strength
- Run both compression and tension experiments
 - yield strength may be higher in compression
- Look for effects of radiation hardening
 - run tests on ‘aged’ samples
 - ^3He bubble voids may be problematic



What's next?

- Details on actuator
 - look for & fix showstoppers
 - check actuation in presence of frozen DT
 - we need a modified electrical connector
- Details on piezo detector
 - check for effects of beta deposition
 - fixes: epoxy coating, grounding of posts, etc.
- Complete design of cell
 - thermal modeling of layer formation
 - Specify/design electrical feed-thrus
- Redesign cryostat if necessary
 - this assembly may be too long for existing apparatus
- Keep at it!!